

GEOTECHNICAL ENGINEERING REPORT RETAINING WALLS STUDY GILCREASE MUSEUM ROAD WIDENING TULSA, OKLAHOMA KLEINFELDER PROJECT NO.: 20230052.006A

MARCH 31, 2023

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A Report Prepared for:

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GEOTECHNICAL ENGINEERING REPORT RETAINING WALLS STUDY GILCREASE MUSEUM ROAD WIDENING TULSA, OKLAHOMA

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March 31, 2023 Kleinfelder Project No. 20230052.006A

Ms. Cynthia Y. Lynn, President Thunderhead Testing, LLC 1540 N. 107th E. Ave., Tulsa, Oklahoma 74116

Subject: Geotechnical Engineering Report Retaining Walls Study Gilcrease Museum Road Widening Tulsa, Oklahoma

Dear Ms. Lynn:

Kleinfelder has completed the authorized subsurface exploration and geotechnical engineering evaluations for the above-referenced project. The purpose of the geotechnical study was to explore and evaluate the subsurface conditions and provide geotechnical recommendations for the proposed retaining walls along the Gilcrease Museum Road in Tulsa, Oklahoma. The attached Kleinfelder report contains a description of the findings of our field exploration and laboratory testing program, our engineering interpretation of the results with respect to the project characteristics, and our geotechnical site development recommendations as well as construction guidelines for the planned project

Recommendations provided herein are contingent on the provisions outlined in the ADDITIONAL SERVICES and LIMITATIONS sections of this report. The project Owner should become familiar with these provisions in order to assess further involvement by Kleinfelder and other potential impacts to the proposed project.

We appreciate the opportunity to be of service to you on this project and are prepared to provide the recommended additional services. Please call us if you have any questions concerning this report.

Sincerely,

KLEINFELDER, INC. *Certificate of Authorization #7292, Expires 6/30/23*

Yicheng Zhang, PE

Project Professional

Shiyun (Simon) Wang, PE Senior Professional

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1	Site Location Diagram
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APPENDICES

- A Field Exploration Program
- B Laboratory Testing Program
- C GBA Document

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GEOTECHNICAL ENGINEERING REPORT RETAINING WALLS STUDY GILCREASE MUSEUM ROAD WIDENING TULSA, OKLAHOMA

1. INTRODUCTION

1.1 GENERAL

Kleinfelder has completed the authorized subsurface explorations and geotechnical engineering evaluations for the proposed retaining walls associated with the roadway widening project along the Gilcrease Museum Road in Tulsa, Oklahoma. The services provided were in general accordance with the work order dated January 24, 2023.

This report includes our recommendations related to the geotechnical aspects of the project design and construction. Recommendations presented in the report are based on the subsurface information encountered at the locations of our exploration and the provisions and requirements outlined in the ADDITIONAL SERVICES and LIMITATIONS sections of this report. In addition, an article prepared by The Geoprofessional Business Association (GBA), *Important Information About This Geotechnical Engineering Report*, has been included in Appendix D. We recommend that all individuals read the report limitations along with the included GBA document.

1.2 PROPOSED CONSTRUCTION

We understand that the City of Tulsa (City) is planning to widen the existing Gilcrease Museum Road from Edison Street extending north approximately one mile to W. Pine Street. As part of the project, three retaining walls are proposed, one on the west side of Gilcrease Museum Road up to the Newton Street intersection (Wall 'A'); one on the west side of Gilcrease Museum Road north of Newton Street (Wall 'B'); and one on the east side of Gilcrease Museum Road north of Newton Street (Wall 'B'); exact locations, and geometries of the retaining walls had not been determined at the time of this report. General locations of the proposed walls and boring locations were provided to Kleinfelder.



Based on the preliminary retaining wall plans prepared by Poe & Associates Inc., retaining wall 'A' will be approximately 1,220 feet long (Station 10+25 to Station 22+45). The wall will be constructed in cut sections and will have a maximum height of approximately 18 feet.

Retaining wall 'B' will be approximately 900 feet long (Station 30+30 to Station 39+30). Wall 'B' will be constructed in both cut and fill sections and will have a maximum wall height of approximately 12 feet.

Retaining wall 'C' will be approximately 1,130 feet long (Station 50+30 to Station 61+60). Wall 'C' will be constructed in both cut and fill sections and will have a maximum wall height of approximately 11 feet.

After the conference call between City of Tulsa (project owner), Poe & Associates (project designer), and Kleinfelder (geotech engineer of record) on March 14, 2023, we understand the following:

- Wall 'A' will be either a soil nail wall or a soldier pile wall depending upon the availability of right of way. No soil nails will be installed inside private properties.
- The southern portion (approximately 300 feet) of Wall 'B' will be soldier pile walls and the remainder will be conventional CIP (cast-in-place) retaining walls.
- Wall 'C' will be a conventional CIP (cast-in-place) retaining wall.

The scope of the exploration and engineering evaluation for this study, as well as the recommendations in this report, were based on our understanding of the project as described above. If pertinent details of the project have changed or otherwise differ from our descriptions, we must be notified and engaged to review the changes and modify our recommendations, if needed.



2. SITE CONDITIONS

2.1 SITE DESCRIPTION

The general location of the project site is shown on Figure 1, Site Location Diagram. South of Newton Street, the project site is surrounded by heavily wooded steep slopes to the east and wooded areas and residential areas to the west. North of Newton Street, the project site is surrounded by residential neighborhood to the east and the Gilcrease Museum to the west.

The existing road is a two-lane, two-direction asphaltic concrete paved roadway with grass and/or gravel shoulders. An existing rock wall, constructed on top of the existing terrain, is present along the west side of the Gilcrease Museum Road north of Newton Street. The height of this wall ranged from 2 to 5 feet. The wall starts from Newton Street and extend north approximately 920 feet to the south side of the Gilcrease Museum entrance. This existing wall appears to be a non-structural rock wall and is located approximately 23 feet west of the centerline of the existing Gilcrease Museum Road.

The site terrain is hilly and generally slopes downward from west to east. The site is lowest in elevation near the Newton Street intersection. Existing overhead and underground utilities were noted along the project alignment. An exposed underground utility was observed at the surface near boring B-15 on the east side of the road. Rock outcroppings were visible at several locations within the project sites.

2.2 GENERAL SITE GEOLOGY

According to the "Engineering Classification of Geological Materials – Division Eight" (1965) by ODOT, the project site appears to be located within the **Coffeyville Unit (Pcf)**. This unit consists predominantly of silty to sandy shale with many thick zones of tan sandstone. The sandstone generally is thin-bedded and moderately hard to soft. Locally, at the base of the unit, a black fissile shale about 15 feet thick is present. The sandstone zones are generally about 15 to 40 feet thick. The total thickness ranges from 175 feet in northern Division 8 to about 500 feet in the south. The Coffeyville Unit outcrops in Creek, Nowata, Rogers, Tulsa, and Washington Counties of Division 8. In Tulsa and Creek Counties, the thick sandstone zones cap prominent scarps.



2.3 SUBSURFACE CONDITIONS

Kleinfelder explored the subsurface conditions by performing a total of 36 borings (B-1 through B-36) between February 6 and 10, 2023. The approximate boring locations are shown onFigures 2 through 5, Boring Location Plan(s). The field exploration and laboratory testing programs are presented in APPENDIX A and APPENDIX B, respectively.

Table 2-1 indicates the ground surface elevations, overburden soils, and the approximate depth and elevation to the top of competent bedrock at the respective boring locations. Depth to competent bedrock is defined as the depth at which the penetration from a Standard Penetration test (SPT), conducted in accordance with ASTM D1586, is less than or equal to 6 inches with 50 blows.

Specific subsurface conditions encountered at the boring locations are presented on the respective boring logs in APPENDIX A. The Subsurface Cross Sections, Figures A-1 through A-3, depict the generalized subsurface profiles across the project sites based on the information obtained from the borings. The stratification lines shown on the logs and subsurface cross sections represent the approximate boundaries between material types; in-situ, the transitions may vary or be gradual.

Table 2-1. Summary of Subsurface Strata							
Walls	Boring No.	Ground Surface Elevation (ft.)	Overburden Soil	Depth to Weathered Bedrock (ft.)	Depth to Competent Bedrock (ft.)	Competent Bedrock	Competent Bedrock Elevation (ft.)
	B-13	804	Sand, Clay, Silt	11	16.0	Shale	788.0
	B-14	813	-	1.0	3.5	Sandstone	809.5
	B-15	827	-	1.0	2.0	Sandstone	825.0
	B-16	836	-	1.0	1.5	Sandstone	834.5
	B-17	843	-	1.0	1.5	Sandstone	841.5
	B-18	847	-	1.0	1.5	Sandstone	845.5
٨	B-19	847	-	1.0	1.5	Sandstone	845.5
A	B-20	850	Silty Sand	-	5.0	Sandstone	845.0
	B-21	846	-	1.0	1.5	Sandstone	844.5
	B-22	849	Sandy Silt	-	4.0	Sandstone	845.0
	B-23	836	-	-	1.0	Sandstone	835.0
	B-24	833	Silty Sand	-	4.0	Sandstone	829.0
	B-25	813	Silty Sand	-	5.0	Sandstone	808.0
	B-26	812	Sandy Silt	-	-	-	-



Table 2-1. Summary of Subsurface Strata							
Walls	Boring No.	Ground Surface Elevation (ft.)	Overburden Soil	Depth to Weathered Bedrock (ft.)	Depth to Competent Bedrock (ft.)	Competent Bedrock	Competent Bedrock Elevation (ft.)
	B-27	812	Silty Sand	4.0	-	-	808.0
	B-28	827	Silty Sand	4.0	9.5	Sandstone	817.5
	B-29	833	-	-	0.5	Sandstone	832.5
	B-30	829	-	-	0.5	Sandstone	828.5
D	B-31	821	Silt	-	4.5	Sandstone	816.5
D	B-32	822	-	0.5	-	Sandstone	821.5
	B-33	825	Silty Sand	4.0	8.5	Sandstone	816.5
	B-34	827	Silt	3.5	8.5	Sandstone	818.5
	B-35	828	Silt	4.0	8.5	Sandstone	819.5
	B-36	827	Silt	4.5	9.0	Sandstone	818.0
	B-1	812	Sandy Silt	-	3.5	Sandstone	808.5
	B-2	816	-	0.5	3.5	Sandstone	812.5
	B-3	819	-	0.5	3.0	Sandstone	816.0
	B-4	820	-	0.5	3.5	Sandstone	816.5
	B-5	820	Sandy Silt	4.0	6.0	Sandstone	814.0
C	B-6	820	Sandy Silt	-	8.0	Sandstone	812.0
Ľ	B-7	820	Sandy Silt	-	6.0	Sandstone	814.0
	B-8	822	-	0.5	3.5	Sandstone	818.5
	B-9	823	-	0.5	3.5	Sandstone	819.5
	B-10	824	-	0.5	4.0	Sandstone	820.0
	B-11	824	-	0.5	4.0	Sandstone	820.0
	B-12	823	-	0.5	4.0	Sandstone	819.0

2.4 GROUNDWATER OBSERVATIONS

No groundwater was observed in the borings during and at end of drilling operations with the exception of Boring B-26. Groundwater was observed at a depth of approximately 5 feet below the existing grade in boring B-26 during drilling operations. However, laboratory moisture characteristics test of the overburden soils indicated high degree of saturation in few of the other boring locations.

The materials encountered in the borings have a wide range of permeabilities, and water level observations over an extended period of time through use of piezometers or cased borings would be required to better define groundwater conditions. Groundwater is likely perched at the bottom of the fill section and above the bedrock, especially during rainy seasons. Fluctuations of groundwater levels can occur due to seasonal variations in the amount of rainfall, runoff, and other factors not evident at the time the borings were performed. The possibility of groundwater level fluctuations should be considered when developing the design and construction plans for the project.



3. GEOTECHNICAL RECOMMENDATIONS

3.1 GENERAL

Based on the results of our field investigation and engineering evaluations, various types of earth retaining structures could be constructed. Conventional cast-in-place retaining wall, soldier pile walls, and soil nail wall options are presented in the following sections.

The recommendations submitted here are based, in part, upon data obtained from our subsurface exploration. The nature and extent of subsurface variations that may exist at the proposed project site will not become evident until construction. If variations appear evident, then the recommendations presented in this report should be evaluated. In the event that any changes in the nature, design, or location of the proposed project are planned, the conclusions and recommendations contained in this report will not be considered valid unless the changes are reviewed, and our recommendations modified in writing.

3.2 CIP (CAST-IN-PLACE) WALLS

3.2.1 General

As mentioned in Section 1.2, it is our understanding that CIP retaining walls may be designed for the north portion of Wall 'B' and entire Wall 'C'. CIP retaining walls can be supported on spread footings for the proposed location along the Gilcrease Museum Road. The bottom of the spread footings should be placed at least 2 feet below the ground surface to avoid frost penetration depth.

3.2.2 Bearing and Sliding Resistance

If chosen, the CIP retaining walls could be supported on shallow footings founded on one foot of compacted fill material to provide a uniform bearing surface. The compacted fill material should be either ODOT Type "A" aggregate base, lean concrete or controlled low strength (CLSM) type of material. Shallow footings should be proportioned using a maximum geotechnical factored bearing resistance of 2,500 psf (pounds per square foot).



The factored bearing resistance (Strength I Limit State) for retaining walls was estimated using a resistance factor 0.45 for sandy soils (AASHTO, 2020). An effective strength friction coefficient of 0.6 (concrete on gravel-sand mixture) could be used to estimate the sliding resistance of the footings and a corresponding resistance factor of 0.80 should be used (AASHTO, 2020). These factors assume that groundwater is at least 2 feet below the footing bearing level.

The same wall section should be supported on similar bearing material, or a construction joint should be installed between the sections that are supported on different materials. Bearing resistance at utility crossings should be evaluated on a case-by-case basis as the project plans are developed.

3.2.3 Lateral Earth Pressure

Active and passive earth pressure coefficients and equivalent fluid density for level backfill conditions are summarized in Table 3-1. The values in Table 3-1 are based on the assumption that the wall will be backfilled with granular and free draining backfill both above the wall footing and within a 1 horizontal to 1 vertical wedge going up from the heel of the wall footing. Passive earth pressures are provided based on the foundation soil properties. When considering passive earth pressures, soils to depths of 2 feet below the ground surface or to the top of footing (whichever is greater) should be ignored.

The static active and passive earth pressure have triangular distribution, with largest load occurring at the bottom of the wall. The typical components of the CIP wall system are presented in Figure 3.1 below.



Figure 3.1: CIP Wall System Components (not to scale)

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The values in Table 3-1 assume that backfill materials of the wedge are free-draining and, therefore, hydrostatic pressures are not included. Adequate drainage must be provided behind the wall for these coefficients to be valid as shown in Figure 3.1. Uniformly distributed vertical surcharge loads should be applied as a uniform (rectangular) distributed pressure with the appropriate corresponding lateral earth pressure coefficient (active).

Table 3-1. Summary of Lateral Earth Pressures – Level Backfill						
	Earth Pressu	re Coefficients	Equivalent Fluid	Density ^{a,b,c} (pcf)		
Backfill Slope	Active	Passive	Active	Passive		
Horizontal	0.3	3.0	38	360		

Notes: H – Horizontal, V – Vertical, pcf – pounds per cubic foot

^a The resultant static active earth pressures act at a height of 0.33 H above the wall base, where H is the height of the wall.

^b Nominal values are provided for earth pressures.

^c Unit weight of granular backfill = 125 pcf; unit weight of foundation soil = 120 pcf

3.2.4 Global Stability

Global stability analysis can be adequately performed once the wall type and configurations are available.

3.2.5 Settlements

Long-term structural settlement for the footings designed and constructed as outlined above should be one inch or less. Differential settlements of approximately one inch or less per 100 feet of wall length should be anticipated. Utility backfill within the wall footprint must be properly compacted to reduce the potential for localized differential settlement.

3.3 SOLDIER PILE WALL

Soldier pile walls are steel H-Piles that are vertically driven or drilled into the ground at regular intervals prior to excavation. As excavation progresses in stages, horizontal lagging (could be timber, steel, or precast concrete panels) is then installed behind the front flanges of H-Piles to retain soils as the excavation continues. The soldier pile walls can be designed as cantilever walls or anchors, or bracing could be installed to provide additional lateral support.



Due to shallow depths to bedrock encountered at the site and the expected wall heights, anchors or bracing are not anticipated for this project. However, pre-drilling may be required for the construction of H-Piles. It should also be noted that cantilever soldier pile size increase dramatically for wall height of 13 feet or greater. It is the sole responsibility of the wall contractor to design the soldier pile wall system.

3.4 SOIL NAIL WALLS

Soil nail walls are typically designed and constructed using a design-build approach by an experienced soil nail wall contractor. The geotechnical engineer typically provides the soil and rock parameters and the preliminary soil nail grout to ground bond stresses to be considered in the design and confirms the global stability meets the required factors of safety. Final wall design should be based on the results of verification load testing performed on several sacrificial test anchors prior to production soil nail installation and wall construction. The geotechnical engineer should select the locations for verification test nails.

After evaluation, a soil nail grout to ground bond stress of 50 psi could be considered in the preliminary design of the soil nail walls. This recommended soil nail grout to ground bond stress is dependent not only upon the bedrock conditions, but also the quality of materials and installation methods, which are the responsibility of the contractor. The bond stress and pullout resistance achieved from the contractor's means and methods should be verified by testing during construction. If necessary, the pullout resistance can be improved by using larger diameter drill holes and/or other grouting methods (e.g., pressure grouting or secondary grouting). Casing the drilled holes for soil nails may be necessary depending on the construction methods or sequencing to prevent caving in the existing soils. The soil nail grout should be placed using a tremie from the bottom of the drilled hole to the top in order to construct a continuously bonded soil nail.

The soil nail wall designer should design a drainage system to prevent hydrostatic pressures from occurring behind the soil nail wall facing, to limit the soaking of soil behind the soil nail wall face and prevent piping or erosion of soil from behind the soil nail wall. The drainage system usually includes a gutter constructed along the crest of the wall, geo-composite strip drains spaced intermittently behind the soil nail wall facing that are connected into weepholes, and/or manifolds/pipes to discharge water away from the bottom of the soil nail wall.



Based on PTI (2014), permanent soil nails should be designed using Class I (encapsulated tendon) corrosion protection. Corrosion protection for grout and other elements should be considered in the design.

Design, construction, and soil nail testing (i.e., verification, proof and performance testing) should be in accordance with PTI (2014) guidance. Plans and specifications should be reviewed by the Geotechnical Engineer. The Geotechnical Engineer or their representative should observe the soil nail installation and testing, and construction.

Deflection monitoring of the soil nail wall during construction is recommended where there are existing structures or utilities that could be impacted by up to ½-inch of lateral or vertical displacement. Deflection monitoring should be performed weekly during construction for horizontal and vertical movement to an accuracy of 0.01 feet. Following completion of wall construction, the monitoring can be discontinued when two consecutive optical survey measurements taken at least one week apart show no horizontal or vertical movements greater than the precision of the survey method.

3.5 SEISMIC HAZARDS DETERMINATION

We have evaluated the seismic hazards based in the 2020 AASHTO LRFD Bridge Design Specification, 9th Edition. Based on our subsurface information and evaluation of the data, we recommend a Site Class "C" be used in design.



4. SITE DEVELOPMENT

4.1 CLEARING AND GRUBBING

Clearing and grubbing should be performed in accordance with the more stringent of the procedures outlined in this section or as specified by the Oklahoma Department of Transportation (ODOT) "Standard Specifications for Highway Construction (2019)", Section 201. We recommend that all unsuitable materials be removed from the site prior to select fill being placed. We recommend that qualified engineering personnel monitor the stripping operations to observe that all unsuitable materials have been removed. Soils removed during stripping operations could be wasted outside of the project site. Care should be exercised to separate these materials to avoid incorporation of the organic matter in structural fill sections.

Care should be taken during required tree excavations to thoroughly remove all root systems from the proposed construction area. Materials disturbed during removal of stumps should be undercut and replaced with structural fill.

4.2 UTILITIES, STORM DRAINS, AND CULVERTS

Relocation of any existing utility lines within or below the foundation and/or active zone should also be completed as part of the site preparation. The lines should be relocated to areas outside the footprint of the proposed retaining walls. We recommend the proposed relocation of the utilities, if any, be completed prior to the beginning of the wall construction. Additionally, any temporary trench excavation for placement or maintenance of utilities within one wall height in front of the wall or two wall heights behind the face should be designed by an engineer who has reviewed this report and the final retaining wall design.

Excavations created by removal of the existing lines or relocating new lines should be cut wide enough to allow for use of heavy construction equipment to compact the backfill. As an alternative, the excavations could be backfilled with Controlled Low Strength Material (CLSM). In addition, the base of the excavations should be thoroughly evaluated by a geotechnical engineer or engineering technician prior to placement



of backfill. All backfill should be placed in accordance with the recommendations presented in Section 4.6 of this report.

Note that utilities, storm drains, and culverts constructed within or below the active zone of soldier pile walls create difficulty in the placement of reinforcement elements and reinforced fill and may require demolition of the wall structure for maintenance/repair. Utilities constructed in or below the active zone may introduce water flow in-excess of the wall drainage capabilities, resulting in wall distress or failure. Where necessary, utilities, storm drains, and culverts should cross perpendicular to the wall face, and backfill around the utility should be closely monitored for proper compaction.

The wall designer should incorporate slip joints into the wall at utility, storm drains, or culvert crossings that may create localized differential settlement (large diameter storm sewers, box culverts, etc.). The civil engineer should consider the potential impact of differential settlement when designing utilities, storm drains, and culverts that are near the proposed retaining wall and incorporate design measures to reduce the risk of leakage from these structures. These storm drains and culverts should be inspected regularly for leaks and any leaks should be promptly repaired.

4.3 MOISTURE CONDITIONING AND COMPACTION

Prior to placement of any required fill, the moisture content of the exposed subgrade should be evaluated. Depending on the in-situ moisture content of the subgrade exposed, moisture conditioning of the exposed grade may be required prior to proof rolling and/or fill placement. The moisture content of the exposed grade in these fill areas should be adjusted to within the range recommended for structural fill, to allow the exposed material to be compacted to a minimum of 95 percent of the Standard Proctor maximum dry density.

Extremely wet or unstable areas that hamper compaction of the subgrade may require undercutting and replacement with structural fill or other stabilization techniques. Suitable structural fill should be placed to reach the design grade as soon as practical after reworking the subgrade to avoid moisture changes in the underlying soils.



4.4 TEST ROLLING (PROOF ROLLING)

Following moisture conditioning, it is recommended that the exposed subgrade for the CIP walls be test rolled. Test Rolling should be performed in accordance with the Oklahoma Department of Transportation (ODOT) "Standard Specifications for Highway Construction (2019)" Section 203.

4.5 EXCAVATIONS

4.5.1 General

It is anticipated that excavations will be in mostly native granular soils, and in weathered and competent sandstone and siltstone bedrock. Excavation of the native soils should be possible with conventional heavy equipment such as backhoes, loaders, etc. Excavations for the retaining walls, recommended permanent underdrain system, and for wall foundation ground improvement should anticipate shallow to surface bedrock. Excavation of the bedrock in confined excavations such as trenches will be difficult and will likely require the use of hydraulic breakers or other rock excavation techniques.

4.5.2 Foundation and Utility Excavations and Slopes

Excavations should be cut to a stable slope or be temporarily braced, depending on the excavation depths and the subsurface conditions encountered. *Temporary construction slopes should be designed in strict compliance with the most recent governing regulations.* The contractor should also be aware that slope height, slope inclination, or excavation depths (including utility trench excavations) should in no case exceed those specified in local, State and/or federal safety regulations, such as OSHA Health and Safety Standard for Excavations, 29 CFR Part 1926, or successor regulations.

Construction slopes should be closely observed for signs of mass movement: tension cracks at the crest, bulging at the toe, etc. If potential stability problems are observed, a geotechnical engineer should be contacted immediately. *The responsibility for excavation safety and stability of temporary construction slopes lies solely with the contractor.* Shoring, bracing, or underpinning may be required to provide structural stability and to protect personnel working within the excavation.



4.5.3 Construction Considerations

Stockpiles and equipment should be placed well away from the edge of excavations and their height should be controlled so they do not surcharge the sides of excavations. Surface drainage should be carefully controlled to prevent the flow of water into excavations.

4.6 STRUCTURAL FILL

4.6.1 Materials

Granular backfill is recommended for the backfill of the CIP walls (within the wedge of approximately 1 horizontal to 1 vertical extending up from the footing at the base of the wall). All granular backfill material should be prepared or meet the properties of the materials specified in Section 703.07 of ODOT 2019 Standard Specification.

The shallow footings of CIP retaining walls should be supported on one foot of compacted fill material to provide a uniform bearing surface. The compacted fill material should be either ODOT Type "A" aggregate base, lean concrete or controlled low strength (CLSM) type of material.

Structural fill required to achieve design grades at other locations should consist of approved materials, free of organic matter and debris. Other than specified above, structural fill placed should consist of a non-plastic to lower plasticity soil with a maximum Plasticity Index (PI) of 22, as determined by the Atterberg limits test ASTM D4318, wet preparation procedure.

4.6.2 Compaction Criteria

Fill should be placed in lifts having a maximum loose lift thickness of 9 inches. The lift thickness may need to be reduced, depending upon the type/size of compaction equipment utilized at the site. All fill placed at the site should be compacted to a minimum of 95 percent of the material's Maximum Dry Density (MDD) as determined by ASTM D698 (Standard Proctor compaction). Moisture contents of the fill at the time of compaction should be maintained within the range as specified in Table 4-1 until completion of the subgrade preparation.

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Table 4-1. Compaction Criteria						
Material	Required Moisture Content (%)	Percent Compaction (%)				
PI > 22	0% to 4% point above optimum	95% of MDD				
PI < = 22	Within 2% point from optimum	95% of MDD				

4.6.3 Existing Onsite Soils

Based on the conditions encountered in the borings, it appears that the onsite soils are suitable for use as general embankment fill, but not as the select backfill behind the proposed retaining walls. Additional field testing is required to verify if the existing onsite soils are used as structural fill.

4.6.4 Organic Soils

Topsoil and more highly organic soils removed during site preparation could be utilized in the upper portion of the fill sections in landscaped areas of the site. Depth of organic fill and degree of compaction should be established to provide a stable surface that will be conducive to the growth of grass cover.



5. ADDITIONAL SERVICES

5.1 PLANS AND SPECIFICATIONS REVIEW

We recommend that Kleinfelder conduct a general review of the final plans and specifications to evaluate that our recommendations have been properly interpreted and implemented during design. In the event Kleinfelder is not retained to perform this recommended review, we will assume no responsibility for misinterpretation of our recommendations.

5.2 CONSTRUCTION OBSERVATION AND TESTING

We recommend that all earthwork and retaining wall installation be monitored by a representative from Kleinfelder, including site preparation, excavation, and placement of all engineered fill. The purpose of these services would be to provide Kleinfelder the opportunity to observe the subsurface conditions encountered during construction, evaluate the applicability of the recommendations presented in this report to the subsurface conditions encountered, and recommend appropriate changes in design or construction procedures if conditions differ from those described herein.



6. LIMITATIONS

This work was performed in a manner consistent with that level of care and skill ordinarily exercised by other members of Kleinfelder's profession practicing in the same locality, under similar conditions and at the date the services are provided. Our conclusions, opinions, and recommendations are based on a limited number of observations and data. It is possible that conditions could vary between or beyond the data evaluated. Kleinfelder makes no other representation, guarantee, or warranty, express or implied, regarding the services, communication (oral or written), report, opinion, or instrument of service provided. The scope of our services did not include any environmental assessment or exploration for the presence of hazardous or toxic materials in the soil, surface water, groundwater, or air, on, below, or around this site.

This report may be used only by the Client and the registered design professional in responsible charge and only for the purposes stated for this specific engagement within a reasonable time from its issuance, but in no event later than two (2) years from the date of the report. Land use, site conditions (both on-site and off-site), regulations, or other factors may change over time, and additional work may be required with the passage of time. Any party other than the client who wishes to use this report shall notify Kleinfelder of such intended use. Based on the intended use of the report, Kleinfelder may require that additional work be performed and that an updated report be issued. Non-compliance with any of these requirements by the Client or anyone else will release Kleinfelder from any liability resulting from the use of this report by any unauthorized party and the client agrees to defend, indemnify, and hold harmless Kleinfelder from any claim or liability associated with such unauthorized or non-compliance.

The work performed was based on project information provided by the Client. If the Client does not retain Kleinfelder to review any plans and specifications, including any revisions or modifications to the plans and specifications, Kleinfelder assumes no responsibility for the suitability of our recommendations. In addition, if there are any changes in the field to the plans and specifications, the Client must obtain written approval from Kleinfelder's engineer that such changes do not affect our recommendations. Failure to do so will vitiate Kleinfelder's recommendations.





The information included on this graphic representation has been compiled from a variety of sources and is subject to change without notice. Reinfelder makes no representations or warranties, express or implied, as to accuracy, completeness, timeliness, or rights to the use of such information. This document is not intended for use as a land survey product nor is it designed or intended as a construction design document. The use or misuse of the information contained on this graphic representation is at the sole risk of the party using or misusing the information.



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RETAINING WALL STUDY GILCREASE MUSEUM RD/S. 25TH W. AVE WIDENING TULSA, OKLAHOMA













FIELD EXPLORATION PROGRAM

Kleinfelder conducted the field work for this study between February 6 and 10, 2023. The exploration consisted of 36 borings drilled to a maximum depth of 35 feet below existing grade. Boring locations were established in the field by a representative of Kleinfelder. A GPS unit was used to locate the exploration with an accuracy of less than 15 feet. Approximate elevations at the boring locations were estimated by Kleinfelder with Plan and Profile drawings prepared by Poe & Associates Inc. Locations and elevations of the borings should be considered accurate only to the degree implied by the methods used. The GPS coordinates and approximate elevations are shown on the top left corner of the boring logs.

The borings were performed with a rubber tire ATV-mounted drill rig (CME-550X) and a track ATV (Diedrich D-50) using solid stem augers. Soil samples were obtained utilizing Standard Penetration test (SPT) method using a 2-inch split-barrel sampler. Split-barrel sampling was conducted in general accordance with ASTM D1586. The split-barrel sampler is driven into the bottom of the boring over an 18-inch sampling interval by a 140-pound hammer that is dropped from a distance of 30 inches. The SPT N-value, recorded on the boring logs, is the number of blows required to drive the split-barrel sampler the final 12 inches of the 18-inch sampling interval. The samples were sealed and returned to our laboratory for further examination, classification, and testing. The borings were backfilled in accordance with the appropriate Oklahoma Water Resources Board Regulations. The weathered bedrock encountered in the borings were also evaluated through use of SPT.

Boring logs included in this Appendix present such data as soil and bedrock descriptions, relative density, consistency, and hardness evaluations, depths, sampling intervals, and observed groundwater conditions. Conditions encountered in each of the borings were monitored and recorded by the drill crew and field professional. Field logs included visual classification of the materials encountered during drilling, as well as drilling characteristics. Our final boring logs represent the engineer's interpretation of the field logs combined with laboratory observation and testing of the samples. Visual classifications were made in accordance with the Unified Soil Classification System presented on the Graphics Key, Soil Description Key and Rock Description Key that are also presented as figures (Figures A-4, A-5, and A-6) in this appendix. The Subsurface Cross Sections, Figures A-1 through A-3, depict the generalized subsurface profiles along the approximate alignments of the proposed retaining walls based on the information obtained from the



borings for each wall. Stratification boundaries indicated on the boring logs and cross sections were based on observations during our field work, an extrapolation of information obtained by examining samples from the borings, and comparisons of soils with similar engineering characteristics. Locations of these boundaries are approximate, and the transitions between material types may be gradual rather than clearly defined.

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DRILLING METHOD/SAMPLER TYPE GRAPHICS		UNIFIED SOIL CLASSIFICATION SYSTEM ¹							
SOLID STEM AUGER			(a	CLEAN GRAVEL		GW	WELL-GRADED GRAVEL, WELL-GRADED GRAVEL WITH SAM	۱D	
(2 in. (50.8 mm.) outer diameter and 1-3/8 in. (34.9 mm.) inner diameter)			o. 4 Sieve	WITH <5% FINES		GP	POORLY GRADED GRAVEL, POORLY GRADED GRAVEL WITH S	SAND	
$\frac{\textbf{GROUND WATER GRAPHICS}}{\nabla}$			on N		Î			г.	
WATER LEVEL (level where hist observed)			ned			GW-GM	WELL-GRADED GRAVEL WITH SIL	r, F AND SAND	
WATER LEVEL (level alter stabilizing period)			retai				WELL-GRADED GRAVEL WITH CLA	AY (OR SILTY	
			ction	GRAVELS		GW-GC	CLAY), WELL-GRADED GRAVEL WI SAND (OR SILT CLAY AND SAND)	ITH CLAY AND	
NOTES	ata		oarse fra	5% TO 12% FINES		GP-GM	POORLY GRADED GRAVEL WITH S POORLY GRADED GRAVEL WITH S	SILT, SILT AND SAND	
and interpretations in this log are subject to the explanations and limitations stated in the report.		ieve)	50% of co			GP-GC	POORLY GRADED GRAVEL WITH C CLAY), POORLY GRADED GRAVEL	CLAY (OR SILTY WITH CLAY AND	
 Solid lines separating strata on the logs represent approximate boundaries only, dashed lines are inferred or extrapolated boundaries. Actual transitions may be gradual or differ from those represented. 		lo. 200 S	ore than 5			GM	SILTY GRAVEL,		
 No warranty is provided as to the continuity of soil or rock conditions between individual sample locations. 	;	l on N	S (Mc	GRAVELS					
• Logs represent general soil or rock conditions observed at the point exploration on the date indicated.	of	retained	SAVELS	WITH > 12% FINES		GC	CLAYEY GRAVEL, CLAYEY GRAVEL WITH SAND		
 In general, Unified Soil Classification System (ASTM D2488/D2487) designations presented on the logs were based on visual classification the field and were modified where appropriate based on gradation and index property testing. 	in	than 50%	Ū			GC-GM	SILTY, CLAYEY GRAVEL SILTY, CLAYEY GRAVEL WITH SAN	ID	
 Fine grained soils that plot within the hatched area on the Plasticity Chart, and coarse grained soils with between 5% and 12% passing the 200 sieve require dual USCS symbols, ie., CL-ML, GW-GM, GP-GM, CL-ML, GW-GM, GP-GM, GW-GM, GP-GM, GW-GM, GP-GM, GW-GM, GP-GM, GW-GM, GW-G	No.	S (More		CLEAN SANDS		sw	WELL-GRADED SAND, WELL-GRADED SAND WITH GRAVI	EL	
 GW-GC, GP-GC, GC-GM, SW-SM, SP-SM, SW-SC, SP-SC, SC-SM. If sampler is not able to be driven at least 6 inches then 50/X indicate number of blows required to drive the identified sampler X inches with a 140 series descence feature 20 inches 	es a	IED SOIL	. 4 Sieve)	<5% FINES		SP	POORLY GRADED SAND, POORLY GRADED SAND WITH GRA	AVEL	
ABBREVIATIONS WOH - Weight of Hammer		E GRAIN	s the No.			SW-SM	WELL-GRADED SAND WITH SILT, WELL-GRADED SAND WITH SILT A	ND GRAVEL	
WOR - Weight of Rod <u>REFERENCES</u> 1. American Society for Materials and Testing (ASTM), 2011, ASTM D2487: Classification of Soils for Engineering Purposes (Unified Soil Classification Contention		COARS	ion passe	SANDS WITH		SW-SC	WELL-GRADED SAND WITH CLAY WELL-GRADED SAND WITH CLAY (OR SILTY CLAY AND GRAVEL)	(OR SILTY CLAY), AND GRAVEL	
Classification System).			arse fract	5% TO 12% FINES		SP-SM	POORLY GRADED SAND WITH SIL POORLY GRADED SAND WITH SIL	T, T AND GRAVEL	
			SANDS (50% or more of co			SP-SC	POORLY GRADED SAND WITH CLA POORLY GRADED SAND WITH CLA (OR SILTY CLAY AND GRAVEL)	AY, AY AND GRAVEL	
				SANDS WITH > 12% FINES		SM	SILTY SAND, SILTY SAND WITH GRAVEL		
					SANDS WITH > 12% FINES		SC	CLAYEY SAND, CLAYEY SAND WITH GRAVEL	
						SC-SM	SILTY, CLAYEY SAND, SILTY, CLAYEY SAND WITH GRAVE	EL	
						ML	SILT, SILT WITH SAND, SILT WITH GRAVEL		
			(e)	SILTS AND	CLAYS	СГ	LEAN CLAY, LEAN CLAY WITH SAND, LEAN CLAY	WITH GRAVEL	
			siev	(Liquid L less thar	Limit n 50)	CL-N	IL SILTY CLAY, SILTY CLAY WITH SAND, SILTY CLAY	WITH GRAVEL	
			#200				ORGANIC CLAY, ORGANIC CLAY WITH SAND, ORG ORGANIC SILT, ORGANIC SILT WITH SAND, ORGA	GANIC CLAY WITH GRAVEL, NIC SILT WITH GRAVEL	
		GR	No.			M	ELASTIC SILT. ELASTIC SILT WITH SAND, ELASTIC	SILT WITH GRAVEL	
			th€	Liquid L 50 or are	Limit ater)	CH	FAT CLAY, FAT CLAY WITH SAND, FAT CLAY WITH	1 GRAVEL	
		NOTE PRO	E: USE	E MATERIA ON THIS			ORGANIC CLAY, ORGANIC CLAY WITH SAND, ORC ORGANIC SILT, ORGANIC SILT WITH SAND, ORGANIC ON THE LOG TO DEFINE A GRAPHIC	SANIC CLAY WITH GRAVEL, INIC SILT WITH GRAVEL	
	PROJI 20230	ECT N	IO.: 06A				GRAPHICS KEY	FIGURE	
		VN RY	·	Y7					
Bright People. Right Solutions.			RV.	QVIN/	25	5th W. Av	enue Widening Retaining Walls	A-4	
DATE		DATE: 3/30/2023		3/30/2023	Tulsa, Oklahoma				

GRAIN S	
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SECONDARY CONSTITUENT¹

DESCF	RIPTION	SIEVE SIZE	GRAIN SIZE	
Boulders	6	>12 in.	>12 in. (304.8 mm.)	
Cobbles		3 - 12 in.	3 - 12 in. (76.2 - 304.8 mm.)	
Crowal	coarse	3/4 -3 in.	3/4 -3 in. (19 - 76.2 mm.)	
Gravel	fine #4 - 3/4 in.		0.19 - 0.75 in. (4.8 - 19 mm.)	
	coarse	#10 - #4	0.079 - 0.19 in. (2 - 4.9 mm.)	
Sand	medium	#40 - #10	0.017 - 0.079 in. (0.43 - 2 mm.)	
	fine	#200 - #40	0.0029 - 0.017 in. (0.07 - 0.43 mm.)	
Fines		Passing #200	<0.0029 in. (<0.07 mm.)	

	AMC	DUNT
Term of Use	Secondary Constituent is Fine Grained	Secondary Constituent is Coarse Grained
Trace	<5%	<15%
With	≥5 to <15%	≥15 to <30%
Modifier	≥15%	≥30%

PLASTICITY¹

DESCRIPTION	CRITERIA
Non-Plastic	A 1/8 in. (3 mm) thread cannot be rolled at any water content.
Low	The thread can barely be rolled and the lump cannot be formed when drier than the plastic limit.
Medium	The thread is easy to roll and not much time is required to reach the plastic limit. The thread cannot be rerolled after reaching the plastic limit. The lump crumbles when drier than the plastic limit.
High	It takes considerable time rolling and kneading to reach the plastic limit. The thread can be rerolled several times after reaching the plastic limit. The lump can be formed without crumbling when drier than the plastic limit.

CONSISTENCY - FINE-GRAINED SOIL^{2,3}

MOISTURE CONTENT¹

DESCRIPTION	FIELD TEST
Dry	Absence of moisture, dusty, dry to the touch
Moist	Damp but no visible water
Wet	Visible free water, usually soil is below water table

APPARENT DENSITY -COARSE-GRAINED SOIL²

SPT-N

(# blows / ft)

<4 4 - 10

>50

-					
APPARENT DENSITY	UNCONFINED COMPRESSIVE STRENGTH (Q,)(psf)		Pocket Pen (tsf)	SPT - N (# blows / ft)	CONSISTENCY
Very Loose	< 0.25 <500 Easily penetrated several inches by fist		PP < 0.25	<2	Very Soft
Loose	Easily penetrated several inches by thumb	500 - 1,000	0.25 <u>≤</u> PP <0.5	2 - 4	Soft
Medium Dense	1,000 - 2,000 Can be penetrated several inches by thumb wit moderate effort		0.5 <u>≤</u> PP <1	4 - 8	Medium Stiff
Dense	Readily indented by thumb but penetrated only				
Very Dense	with great effort	2,000 - 4,000	1 <u>≤</u> PP <2	8 - 15	Stiff
	Readily indented by thumbnail	4,000 - 8,000	2 <u>≤</u> PP <4	15 - 30	Very Stiff
	Indented by thumbnail with difficulty	>8,000	4 ≤ PP	>30	Hard

STRUCTURE¹

REFERENCES

Manual Procedures).

Practice, John Wiley & Sons, New York.

(USBR), 1998, Earth Manual, Part I.

DESCRIPTION	CRITERIA
Stratified	Alternating layers of varying material or color with layers at least 1/4-in. (6mm) thick, note thickness.
Laminated	Alternating layers of varying material or color with the layers less than 1/4-in. (6 mm) thick, note thickness.
Fissured	Breaks along definite planes of fracture with little resistance to fracturing.
Slickensided	Fracture planes appear polished or glossy, sometimes striated.
Blocky	Cohesive soil that can be broken down into small angular lumps which resist further breakdown.
Lensed	Inclusion of small pockets of different soils, such as small lenses of sand scattered through a mass of clay; note thickness.
Homogeneous	Same color and appearance throughout

1. American Society for Materials and Testing (ASTM), 2017, ASTM D2488: Standard Practice for Description and Identification of Soils (Visual

2. Terzaghi, K and Peck, R., 1948, Soil Mechanics in Engineering

3. United States Department of the Interior Bureau of Reclamation

ANGULARITY¹

DESCRIPTION	CRITERIA
Angular	Particles have sharp edges and relatively plane sides with unpolished surfaces.
Subangular	Particles are similar to angular description but have rounded edges.
Subrounded	Particles have nearly plane sides but have well-rounded corners and edges.
Rounded	Particles have smoothly curved sides and no edges.

REACTION WITH HYDROCHLORIC ACID¹

CEMENTATION¹

DESCRIPTION	FIELD TEST	DESCRIPTION	FIELD TEST
None	No visible reaction	Weakly	Crumbles or breaks with handling or little finger pressure
Weak	Some reaction, with bubbles forming slowly	Moderately	Crumbles or breaks with considerable finger pressure
Strong	Violent reaction, with bubbles forming immediately	Strongly	Will not crumble or break with finger pressure

\bigcap	PROJECT NO.: 20230052.006A		SOIL DESCRIPTION KEY (For additional tables, see ASTM D2488)	FIGURE
KLEINFELDER	DRAWN BY:	YZ	25th W. Avenue Widening Retaining Walls	A-5
Bright People. Right Solutions.	CHECKED BY:	SYW	Gilcrease Museum	
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TED: 03/30/2023 1				
LTED: 03/30/2023 1				
TTED: 03/30/2023 1				

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INFILLING TYPE

	-			
NAME	ABBR	NAME	ABBR	
Albite	AI	Muscovite	Mus	
Apatite	Ар	None	No	
Biotite	Bi	Pyrite	Ру	
Clay	CI	Quartz	Qz	
Calcite	Ca	Sand	Sd	
Chlorite	Ch	Sericite	Ser	
Epidote	Ep	Silt	Si	
Gypsum	Gy	Talc	Та	
Iron Oxide	Fe	Unknown	Uk	
Manganese	Mn			

DENSITY/SPACING OF DISCONTINUITIES⁵

DESCRIPTION	SPACING CRITERIA
Unfractured	>6 ft. (>1.83 meters)
Slightly Fractured	2 - 6 ft. (0.061 - 1.83 meters)
Moderately Fractured	8 in - 2 ft. (203.20 - 609.60 mm)
Highly Fractured	2 - 8 in (50.80 - 203.30 mm)
Intensely Fractured	<2 in (<50.80 mm)

ADDITIONAL TEXTURAL ADJECTIVES⁵

DESCRIPTION	RECOGNITION					
Pit (Pitted)	Pinhole to 0.03 ft. (3/8 in.) (>1 to 10 mm.) openings					
Vug (Vuggy)	Small openings (usually lined with crystals) ranging in diameter from 0.03 ft. (3/8 in.) to 0.33 ft. (4 in.) (10 to 100 mm.)					
Cavity	An opening larger than 0.33 ft. (4 in.) (100 mm.), size descriptions are required, and adjectives such as small, large, etc., may be used					
Honeycombed	If numerous enough that only thin walls separate individual pits or vugs, this term further describes the preceding nomenclature to indicate cell-like form.					
Vesicle (Vesicular)	Small openings in volcanic rocks of variable shape and size formed by entrapped gas bubbles during solidification.					

WEATHERING⁵

DESCRIPTION	CRITERIA					
Unweathered	No evidence of chemical / mechanical alternation; rings with hammer blow.					
Slightly Weathered	Slight discoloration on surface; slight alteration along discontinuities; <10% rock volume altered.					
Moderately Weathered	Discoloring evident; surface pitted and alteration penetration well below surface; Weathering "halos" evident; 10-50% rock altered. Entire mass discolored; Alteration pervading most rock, some slight weathering pockets; some minerals may be leached out.					
Highly Weathered						
Decomposed	Rock reduced to soil with relic rock texture/structure; Generally molded and crumbled by hand.					



RELATIVE HARDNESS / STRENGTH DESCRIPTIONS⁴

	GRADE	UCS	FIELD TEST
R0	Extremely Weak	0.25 - 1.0	Indented by thumbnail
R1	Very Weak	1.0 - 5.0	Crumbles under firm blows of geological hammer, can be peeled by a pocket knife.
R2	Weak	5.0 - 25	Can be peeled by a pocket knife with difficulty, shallow indentations made by firm blow with point of geological hammer.
R3	Medium Strong	25 - 50	Cannot be scraped or peeled with a pocket knife, specimen can be fractured with a single firm blow of a geological hammer.
R4	Strong	50 - 100	Specimen requires more than one blow of geological hammer to fracture it.
R5	Very Strong	100 - 250	Specimen requires many blows of geological hammer to fracture it.
R6	Extremely Strong	> 250	Specimen can only be chipped with a geological hammer.

ROCK QUALITY DESIGNATION (RQD)²

DESCRIPTION	RQD (%)							
Very Poor	0 - 25							
Poor	25 - 50							
Fair	50 - 75							
Good	75 - 90							
Excellent	90 - 100							

APERTURE¹

DESCRIPTION	CRITERIA [in (mm)]
Tight	<0.04 (<1)
Open	0.04 - 0.20 (1 - 5)
Wide	>0.20 (>5)

BEDDING CHARACTERISTICS⁶

Thickness [in (mm)]
>36 (>915)
12 - 36 (305 - 915)
4 - 12 (102 - 305)
1 - 4 (25 - 102)
0.4 - 1 (10 - 25)
0.1 - 0.4 (2.5 - 10)
<0.1 (<2.5)

Bedding Planes Planes dividing the individual layers, beds, or stratigraphy of rocks. Joint Fracture in rock, generally more or

less vertical or traverse to bedding. Applies to bedding plane with unspecified degree of weather.

CORE SAMPLER TYPE GRAPHICS

SYW

3/30/2023



PROJECT NO .:

20230052.006A

DRAWN BY:

CHECKED BY:

DATE:

Seam

JOINT ROUGHNESS COEFFICIENT (JRC)⁴



RQD Rock-quality designation (RQD) Rough measure of the degree of jointing or fracture in a rock mass, measured as a percentage of the drill core in lengths of 4 in. (10 cm.) or more.

REFERENCES 1. Bieniawski, Z.T., 1989, Engineering Rock Mass Classifications. John Wiley & Sons, New York. (Mod. by

Classifications. John Wiley & Sons, New York. (Mod. by Kleinfelder). 2. Deere, D.U., and Deere, D.W., 1989, Rock Quality Designation (RQD) After Twenty Years, USACE Contract Report GL-89-1.

3. Federal Highway Administration (FHWA), 2002, Subsurface Investigations, FHWA-NHI-01-031. (Mod. by Kleinfelder).

A. International Society for Rock Mechanics (ISRM), 1978, "Suggested Methods for the Quantitative Description of Discontinuities in Rock Masses," International Joint Rock Mechanics and Mining Sciences & Geomechanics Abstracts, Vol. 15.

 United States Army Corps of Engineers (USACE), 1994, Rock Foundations, EM 1110-1-2908, November 30, 1994.
 United States Department of the Interior Bureau of Reclamation (USBR), 1998, Engineering Geology Field Manual, Volume 1.



[KLF_GEO_LEG3_ROCK_DESC_KEY] 20230052.006A **PROJECT NUMBER:** GINT_LIBRARY_2023.GLB E:KLF_STANDARD 2023 Klf_gint_master_

TEMPLATE:

gINT FILE:

OFFICE FILTER: TULSA

Zhang	Date Begin - End:						Drilling Company: Aimright Tes										BORING LOG B-1		
	Logged By: B. Goben				B. Goben	Drill Cre	Drill Crew: P. Scarborough												
M B	Hor.	-Vert	. Dat	um:	Not Available	Drilling	Drilling Equipment: Drilling Method:			Diedrich D-50 Solid Flight Auger			Hammer Hammer			ə - Dr	ор: _	140 lb. Auto - 30 in.	
:45 A	Plur	nge:			-90 degrees	Drilling										cienc	y: _	78.7%	
3 10	Wea	ather			Not Available	Explorat	ion Di	iame	ter: 6 in.	D.D.			На	mme	r Cal.	Date	: _:	2/02/2023	
/202					FIELD	EXPLORATION	N						LABORATORY RESULTS						
PLOTTED: 03/3	Approximate Elevation (feet)	Depth (feet)	Graphical Log	Арр	Latitude: 36.17305° N Longitude: -96.01973° E roximate Ground Surface Elevatio Surface Condition: Grass Lithologic Description	on (ft.): 812.0 s	Sample Number	Sample Type	Blow Counts(BC)= Uncorr. Blows/6 in.	Recovery (NR=No Recovery)	USCS Symbol	Water Content (%)	Dry Unit Wt. (pcf)	Passing #4 (%)	Passing #200 (%)	Liquid Limit	Plasticity Index (NP=NonPlastic)	Additional Tests/ Remarks	
	-		<u>x1,</u>	TOP	SOIL: 6 inches			ł				-						-	
	- 	-		Sanc medi SAN	ty SILT (ML) : brown, moist, lo um dense DSTONE : brown and reddish	brown,	SS-1		C=50/4.25"	4"		11.1		100	27			-	
	-	-		extremely weak, weathered															
	-	5-		The I ft. be backt 2023	boring was terminated at app low ground surface. The bor filled with auger cuttings on F	roximately 4 ing was ēebruary 06,						GROU Ground comple <u>GENE</u> The ex estima A Hand accura	NDWA dwater etion. RAL No ploration ted by dheld Co cy of 1	ATER I was n OTES: on loca Kleinfe GPS ur 5 feet.	LEVEL ot obs ation a elder. nit was	<u>INFO</u> erved nd ele	RMATI during vation a to loca	<u>ION:</u> drilling or after are approximate and were te the exploration with an	
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Zhang	Date	e Beg	Ind:	2/06/2023	Drilling Company: Aimright Testing												BORING LOG B-2			
Y: Yi	Log	ged E	By:		B. Goben	Drill Cre	I Crew: <u>P.</u>		P. Sc	P. Scarborough				L						
M B	Hor.	-Vert	. Dat	um:	Not Available	Drilling l	t: Diedr	Diedrich D-50			Hamme			ə - Dr	ор: _	140 lb. Auto - 30 in.				
:45 A	Plur	Plunge:90 degrees Dri				Drilling l	Drilling Method: Solid Flight			Auger Hamm				r Effic	ciency	y: _	78.7%			
23 10	Wea	ther			Not Available	Explorat	ion Di	ame	eter: 6 in. (D.D.			На	mme	r Cal.	Date	: _:	2/02/2023		
1/202					FIELD EX	PLORATION	1							ILTS						
PLOTTED: 03/3	vpproximate Elevation (feet))epth (feet)	Braphical Log	Арр	Latitude: 36.17327° N Longitude: -96.01974° E oroximate Ground Surface Elevation (Surface Condition: Grass	ft.): 816.0	sample Jumber	ample Type	low Counts(BC)= incorr. Blows/6 in.	kecovery NR=No Recovery)	JSCS symbol	Vater Content (%)	Jry Unit Wt. (pcf)	assing #4 (%)	assing #200 (%)	iquid Limit	lasticity Index NP=NonPlastic)	dditional Tests/ temarks		
	¥Ш		0 \\\/	TOP			νz	S S	ШĊ	КĘ	⊃ິ	≤u	Δ	₽.	₽.		⋴∊	<u> ۲</u>		
	-815	-		High	iy Weathered SANDSTONE: bro mely weak	own,														
	-	_		SAN	DSTONE : brown, extremely wea	k	SS-1		BC=50/5.75"	5"		11.1		100	43					
	ŀ	-		The	horing was terminated at approx	imately /				•		GROU			F\/FI		RMATI	ON [.]		
				ft. be	elow ground surface. The boring	was	nately 4 was							was n	ot obs	erved	during	drilling or after		
	-	5—		back 2023	filled with auger cuttings on Feb 8.	ruary 06,							RAL N	OTES:	ation a	nd ele	vation	tion are approximate and were		
												estima	ited by	Kleinfe	ation and elevation are approximate and were elder.					
	-810	-										accura	icy of 1	5 feet.	iit was	useu	lo loca	te the exploration with an		
SA		_																		
: TUI																				
LTER																				
E E	-	-																		
OFFIG																				
_0G]	-	-																		
SOIL L																				
PIT S	-	10-																		
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JMBE B	-	-																		
CT NU																				
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BRAR																				
יד_נוו	ŀ	-																		
GIN																				
3 DARC																				
naster_202 <lf_stani< td=""><td></td><td></td><td></td><td></td><td></td><td>PRO. 2023</td><td>JECT N 0052.00</td><td>10.: 06A</td><td></td><td></td><td></td><td>во</td><td>RING</td><td>GLO</td><td>G B-</td><td>2</td><td></td><td>BORING</td></lf_stani<>						PRO. 2023	JECT N 0052.00	10.: 06A				во	RING	GLO	G B-	2		BORING		
gint_n E: E:ŀ	[~1						BAC											
KIf_(>LATE		n		E / I Brid	aht People, Right Solutions				DAG	2	5th W.	Aven	ue Wi	denin	g Reta	aining	Walls	, В-2		
FILE: TEMF			_		g Copier night solutions.		JKED E	5Y:	SYW			Gi	ulsa, (e Mus Oklah	seum oma					
gINT gINT						DATE	:		3/29/2023									PAGE: 1 of 1		

Zhang	Date	e Beg	in - E	nd:	2/06/2023	Dr	illing	Comp	any:	Aimri	ght Te	sting							BORING LOG B-3
Υ.	Log	ged E	By:		B. Goben	Dr	ill Cre	w:		P. Sc	arboro	ugh			L				
M B	Hor.	-Vert	. Dat	um:	Not Available	Dr	illing	Equip	men	t: Diedr	ich D-	50		На	mme	r Type	ə - Dr	ор: _	140 lb. Auto - 30 in.
):46 <i>P</i>	Plun	ige:			-90 degrees	Dr	illing	Metho	d:	Solid	Flight	Auger		Ha	mme	r Effic	ienc	y: _	78.7%
23 10	Wea	ther			Not Available	Ex	plorat	ion Di	ame	eter: 6 in.	O.D.			На	mme	r Cal.	Date	: _	2/02/2023
31/202					FIE	ELD EXPLO	RATION	N							LA	BORA	TOR	RESU	JLTS
PLOTTED: 03/3	Approximate Elevation (feet)	Jepth (feet)	Sraphical Log	Арр	Latitude: 36.17353 Longitude: -96.019 roximate Ground Surface Ele Surface Condition: (3° N 73° E evation (ft.): 8′ Grass	19.0	Sample Jumber	sample Type	llow Counts(BC)= Jncorr. Blows/6 in.	Recovery NR=No Recovery)	JSCS Symbol	Vater Content (%)	Jry Unit Wt. (pcf)	assing #4 (%)	assing #200 (%)	-iquid Limit	Plasticity Index NP=NonPlastic)	dditional Tests/ Remarks
	ЦШ		<u></u>	TOP	SOIL: 6 inches	puon		02		ШЭ	ШU	0	>0		ш	ш		ЩС	<u>م</u> لا
			KIN.	Link															
	-	-		extre	DSTONE: brown, extreme	elv weak		SS-1		BC=50/4"	4"	-	11.1		100	39			
			<u>···</u> ·							50-30/4									
		_		The I 3.5 ft	ooring was terminated at . below ground surface.	approximate The boring v	ely was						<u>GROU</u> Groun	INDW / dwater	ATER I was n	<u>EVEL</u> ot obs	INFO erved	RMAT during	<u>ION:</u> drilling or after
				back	filled with auger cuttings	on February	06,						comple GENE	etion. RAL N	OTES:				
		-		2023									The exertime	ploration ted by	on loca Kleinfe	ation a elder.	nd ele	vation	are approximate and were
	_	5-											A Hane accura	dheld (icy of 1	SPS ur 5 feet.	nit was	used	to loca	te the exploration with an
	-	-																	
JLSA	-	-																	
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UMBI LB [-	-																	
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ROJE {Y_20	-	-																	
BRAF																			
	805	-																	
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3 DARE																			
aster_202 LF_STAN							PRO 2023	JECT N 0052.00	10.: 06A				BO	RING	GLO	G B-	3		BORING
int_m E:K	[-																	
KIf_g LATE:		K	L	E	NFELDE	R		WN BY	:	BAG	2	5th W.	Aven	ue Wie	denin	g Reta	aining	Walls	₅ B-3
FILE:			_	Brig	gnt reople. Right Solut	tions.	CHE	CKED E	3Y:	SYW			Gi T	lcreas ulsa (e Mu: Oklah	seum oma			
gINT F gINT 7				s : .			DATE	Ξ:		3/29/2023			•						PAGE: 1 of 1

Zhang	Date	e Beç	jin - E	nd:	2/06/2023	Drilling	Comp	any:	Aimri	ght Tes	sting							BORING LOG B-4	
Υ. Υ	Log	ged I	Зу:		B. Goben	Drill Cre	ew:		P. Sc	arborou	ugh			L					_
M B	Hor.	-Ver	t. Dat	um:	Not Available	Drilling	Equip	ment	Diedr	ich D-5	50		Ha	mme	r Type	ə - Dr	op: _	140 lb. Auto - 30 in.	-
0:46 /	Plun	ige:			-90 degrees	Drilling	Metho	od:	Solid	Flight /	Auger		На	mme	r Effic	cienc	y: _	78.7%	-
23 10	Wea	ther			Not Available	Explora	tion Di	iamet	er: 6 in.	0.D.			На	mme	r Cal.	Date	:	2/02/2023	-
31/202					FIELD	EXPLORATIO	N							LA	BORA	TORY	RESL	ILTS	
PLOTTED: 03/3	Approximate Elevation (feet)	Depth (feet)	Graphical Log	Арр	Latitude: 36.17380° N Longitude: -96.01974° E oroximate Ground Surface Elevati Surface Condition: Gras Lithologic Descriptior	: on (ft.): 820.0 s 1	Sample Number	Sample Type	Blow Counts(BC)= Uncorr. Blows/6 in.	Recovery (NR=No Recovery)	USCS Symbol	Water Content (%)	Dry Unit Wt. (pcf)	Passing #4 (%)	Passing #200 (%)	Liquid Limit	Plasticity Index (NP=NonPlastic)	Additional Tests/ Remarks	
			<u>z, 1/</u>	TOP	SOIL: 6 inches			I											
	-	-		High extre	ly Weathered SANDSTONE: mely weak	brown,													-
	_	-						I											
	-	_		SAN ∖weak	DSTONE: light brownish gray	r, extremely /	SS-1	В	C=50/4"	4"		10.5		100	45				_
	-815	5		The I ft. be backi 2023	boring was terminated at app low ground surface. The bor filled with auger cuttings on F	roximately 4 ing was ⁻ebruary 06,						GROU Ground Comple <u>GENE</u> The ex estima A Hand accura	NDWA dwater etion. RAL No ploratio ted by dheld C icy of 1	<u>TER I</u> was n <u>DTES:</u> on loca Kleinfe GPS ur 5 feet.	LEVEL ot obs ation a elder. nit was	<u>INFO</u> erved nd ele used	RMATI during vation to loca	<u>ION:</u> drilling or after are approximate and were te the exploration with an	
OFFICE FILTER: TULSA 0G]	-	-																	
. PIT SOIL LC	-810	10-																	
)052.006A RING/TEST	_	-																	
BER: 2023(KLF_BO	_	_																	
JECT NUMI 2023.GLB		_																	
IBRARY	-	-																	
ARD_GINT_L	_	-																	
master_2023 KLF_STAND						PRO 2023	JECT N 80052.00	NO.: 06A				BO	RING	6 LO	G B-	4		BORING	-
VT FILE: KIf_gint_ VT TEMPLATE: E:				E/I Brig	NFELDEF ght People. Right Solution	S. DRA	WN BY CKED F E:	": BY: 3	BAG SYW 8/29/2023	25	5th W.	Avenı Gi T	ue Wio Icreas ulsa, (dening e Mus Oklah	g Reta seum oma	aining	Walls	B-4	
gll gl																		FAGE: 1011	

iZhang	Date	e Be	gin - I	End:	2/06/2023	Drilling	Comp	oany:	Aimri	ght Te	sting							BORI	NG LOO	G B-5
3Y: Y	Log	ged	By:		B. Goben	Drill Cre	ew:		P. Sc	arboro	ugh			L						
AM B	Hor.	Vei	t. Da	tum:	Not Available	Drilling	Equip	oment	Diedr	ich D-	50		Ha	mme	r Type	e - Dr	ор: _	140 lb. Auto	o - 30 in	<u> </u>
0:46 /	Plur	nge:			-90 degrees	Drilling	Methe	od:	Solid	Flight	Auger		На	mme	r Effic	ciency	/: _	78.7%		
23 1(Wea	athe	:	•	Not Available	Explorat	tion D	Diamet	er: 6 in.	O.D.			На	mme	r Cal.	Date	_	2/02/2023		
31/20:					FIELD EXF	PLORATIO	N							LA	BORA	TORY	RESL	JLTS		
PLOTTED: 03/3	Approximate Elevation (feet)	Depth (feet)	Graphical Log	Ap	Latitude: 36.17406° N Longitude: -96.01974° E proximate Ground Surface Elevation (fi Surface Condition: Grass Lithologic Description	i.): 820.0	Sample Number	Sample Type	Blow Counts(BC)= Uncorr. Blows/6 in.	Recovery (NR=No Recovery)	USCS Symbol	Water Content (%)	Dry Unit Wt. (pcf)	Passing #4 (%)	Passing #200 (%)	Liquid Limit	Plasticity Index (NP=NonPlastic)		Additional Tests/ Remarks	
			<u></u>	TOF	SOIL: 6 inches			T												
	- - 	5-	XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX	Higi	Idy SILT (ML): brown and reddish st, medium dense hly Weathered SILTSTONE: brow emely weak	brown,	SS-1	B	C=9 16 20	18"		14.1		100	54					-
					NDSTONE: brown, extremely weak		158-2	<u>B</u>	C=50/2"											
	SANDSTONE: brown, extremely weak The boring was terminated at approximately 6 ft. below ground surface. The boring was backfilled with auger cuttings on February 06, 2023. GROUND Groundwa completion GENERAL The explo									INDW A dwater etion. <u>RAL Ni</u> ploration ploration ted by dheld C acy of 1	ATER I was n OTES: on loca Kleinfe SPS ur 5 feet.	<u>EVEL</u> ot obso ation a elder. nit was	INFO erved nd ele used	<u>RMAT</u> during vation to loca	<u>ION:</u> drilling or aff are approxin ite the explor	ter nate and ration wit	were h an			
PIT S	-810	10-	4																	
LIBRARY_2023.GLB [_KLF_BORING/TEST	-	_	-																	
ATE: E:KLF_STANDARD_GINT_				E	NFELDER	PRO 2023 DRA	JECT 1 80052.0	NO.: 006A Y:	BAG	25	5th W.	BO	RINC ue Wid	G LO	G B-	5 ainina	Walls	3	BORING	G
gINT TEMPL			-	Br	ight People. Right Solutions.	CHE	CKED E:	BY:	SYW /29/2023			Gi T	lcreas ulsa, (e Mus Oklah	seum oma			PAGE	E: 1	of 1

'iZhang	Date	e Beg	jin - E	End:	2/06/2023	Drilling	Comp	any	: <u>Aimri</u>	ght Te	sting							BORING LOG B-6
ВҮ: Y	Log	ged E	By:		B. Goben	Drill Cro	ew:		P. Sc	arboro	ugh							
AM E	Hor.	-Vert	. Dat	um:	Not Available	Drilling	Equip	mer	nt: Diedr	ich D-	50		Ha	mme	r Тур	e - Dr	op: _	140 lb. Auto - 30 in.
0:46	Plun	ige:			-90 degrees	Drilling	Metho	od:	Solid	Flight	Auger		Ha	mme	r Effic	cienc	y: _	78.7%
123	Wea	ther:			Not Available	Explora	tion D	iam	eter: 6 in. (D.D.			На	mme	r Cal.	Date	: _	2/02/2023
31/20					FIELD	EXPLORATIO	N							LA	BORA	TORY	(RESI	JLTS
PLOTTED: 03/	Approximate Elevation (feet)	Depth (feet)	Graphical Log	Арр	Latitude: 36.17434° N Longitude: -96.01974° E oroximate Ground Surface Elevatic Surface Condition: Grass Lithologic Descriptior	on (ft.): 820.0 S	Sample Number	Sample Type	Blow Counts(BC)= Uncorr. Blows/6 in.	Recovery (NR=No Recovery)	USCS Symbol	Water Content (%)	Dry Unit Wt. (pcf)	Passing #4 (%)	Passing #200 (%)	Liquid Limit	Plasticity Index (NP=NonPlastic)	Additional Tests/ Remarks
			<u>×11/</u>	TOP	SOIL: 6 inches			T										
	-			Sano mois	ty SILT (ML) : brown and redd t, loose	ish brown,			BC=3	18"		14.4		100	50			-
ILIER: IULSA	- 815 -								2 5									-
ц Ц	-			SAN	DSTONE: brown, extremely w	eak	⊥ <u>ss-</u> 2.		BC=50/2.25"	2"								
RD_GINT_LIBRARY_2023.GLB [_KLF_BORING/TEST PIT SOIL LOG]	- 	- 10- - -		The ft. be back 2023	boring was terminated at app low ground surface. The bor filled with auger cuttings on F	roximately 8 ing was ebruary 06,						<u>GROU</u> Groun <u>Comple</u> <u>GENE</u> estima A Han accura	INDWA dwater ation. RAL N/ gloratii ted by dheld C icy of 1	ATER was n OTES: on loc: Kleinfa JPS ur 5 feet.	LEVEL ot obs : ation a elder. it was	<u>INFO</u> erved nd ele	RMAT during	ION: drilling or after are approximate and were ate the exploration with an
E:KLF_STANDA	(PRC 2023	0JECT N 30052.0	NO.: 06A				во	RING	G LO	G B-	6		BORING
gINT FILE: KIT_gI gINT TEMPLATE:				EI. Brij	NFELDEF ght People. Right Solution:	CHE	WN BY	': BY:	BAG SYW 3/29/2023	2	5th W.	Avenı Gi T	ue Wio Icreas ulsa, (dening e Mu Oklah	g Reta seum oma	aining	y Walls	s B-6 PAGE: <u>1 of 1</u>

Zhang	Date	e Beç	jin - E	nd:	2/06/2023	Drilling	Comp	any:	Aimri	ght Te	sting							В	ORING L	.OG B-7
.Υ Υ	Log	ged	Зу:		B. Goben	Drill Cre	ew:		P. Sc	arboro	ugh			l						
M B	Hor.	-Ver	t. Dat	um:	Not Available	Drilling	Equip	men	t: Diedr	ich D-8	50		Ha	Imme	r Type	e - Dr	ор: _	140 lb. /	Auto - 30	in.
0:46 /	Plun	ige:			-90 degrees	Drilling	Metho	od:	Solid	Flight	Auger		Ha	Imme	r Effic	ciency	y: _	78.7%		
23 10	Wea	ther			Not Available	Explora	tion D	iame	eter: 6 in. (D.D.			На	imme	r Cal.	Date	: _	2/02/20	23	
31/202					FIELD E	XPLORATIO	N			_				LA	BORA	TORY	RESU	JLTS		
PLOTTED: 03/3	Approximate Elevation (feet)	Jepth (feet)	Braphical Log	Арр	Latitude: 36.17460° N Longitude: -96.01970° E oroximate Ground Surface Elevation Surface Condition: Grass	n (ft.): 820.0	Sample Jumber	Sample Type	llow Counts(BC)= Jncorr. Blows/6 in.	Recovery NR=No Recovery)	JSCS Symbol	Vater Content (%)	Dry Unit Wt. (pcf)	assing #4 (%)	assing #200 (%)	-iquid Limit	Plasticity Index NP=NonPlastic)		Additional Tests/ Remarks	
	ЧШ			TOP	SOIL: 6 inches		ωZ	S S	ш⊃	щΞ	S	>0		<u> </u>	<u> </u>		чe		<u>م</u> لا	
0.A	- - 	- - 5-		Sanc loose SAN	SUIL: 6 Incres	wet, very	SS-1		BC=WOH WOH WOH BC=50/3"	12"		20.9 <u>GROU</u> <u>Groun</u>	NDW/	100	55	INFO	RMAT	ION: drilling c	r after	-
OIL LOG]	-	-		6.5 ft back 2023	:. below ground surface. The t filled with auger cuttings on Fe	boring was ebruary 06,						GENE GENE The exertima A Hand accura	awater etion. RAL Ne ploration ted by dheld C acy of 1	OTES on loca Kleinfi GPS ui 5 feet.	ation a elder. nit was	nd ele used	vation to loca	are appr	pximate a	nd were with an
. PIT S	-810	10-																		
3 PROJECT NUMBER: 20230052.006A DARD_GINT_LIBRARY_2023.GLB	-	-																		
aster_202 LF_STAN						PRC 2023	JECT N 30052.0	10.: 06A				во	RING	GLO	G B-	7			BOR	ING
jint_m E:K	/		~ .	$ \rightarrow $			14/51		D • 6										-	_
FILE: KIf_g TEMPLATE				E/I Brig	NFELDER ght People. Right Solutions.	CHE	WN BY	': BY:	BAG SYW	2:	ōth W.	Aven Gi T	ue Wie Icreas Julsa, (denin e Mu Oklah	g Reta seum oma	aining	Walls	s	B-	-1
gINT gINT						DAT	E:		3/29/2023									P	AGE:	1 of 1

Zhang	Date	e Beç	gin - E	Ind:	2/06/2023	Drilling (Compa	any:	Aimri	ght Te	sting							BORING LOG B-8
.X	Log	ged	By:		B. Goben	Drill Crev	w:		P. Sc	arboro	ugh			L				
AM B	Hor.	Ver	t. Dat	um:	Not Available	Drilling E	Equip	men	t: Diedr	ich D-5	50		На	mme	r Typ	e - Dr	ор: _	140 lb. Auto - 30 in.
0:46 /	Plur	nge:			-90 degrees	Drilling I	Netho	d:	Solid	Flight	Auger		На	mme	r Effic	cienc	y: _	78.7%
23 1(Wea	ather	:		Not Available	Explorati	ion Di	ame	eter: 6 in. (D.D.			На	mme	r Cal.	Date	: _	2/02/2023
31/20					FIELD EXF	PLORATION	1							LA	BORA	TORY	RESU	JLTS
PLOTTED: 03/3	proximate evation (feet)	spth (feet)	aphical Log	Арг	Latitude: 36.17488° N Longitude: -96.01970° E proximate Ground Surface Elevation (fl Surface Condition: Grass	t.): 822.0	imple imber	imple Type	w Counts(BC)= corr. Blows/6 in.	covery R=No Recovery)	SCS mbol	ater intent (%)	y Unit Wt. (pcf)	ıssing #4 (%)	Issing #200 (%)	quid Limit	asticity Index P=NonPlastic)	lditional Tests/ smarks
	ЧР	De	ō		Lithologic Description		Sa Nu	Sa	Duc	₽Z	Sy Sy	Χö	D	Ра	Ра	Lic	₫Z	Ad Re
			<u>×' //</u>	TOP	SOIL: 6 inches			I										
	- 			High extre	n ly Weathered SANDSTONE : bro emely weak	wn,												-
	-	-		SAN	DSTONE: brown, extremely weak	ζ	SS-1		BC=50/5"	5"		9.4		100	21			-
	ŀ		[The	boring was terminated at approvi	mately 4						GROI			F//FI		RMAT	ION
				ft. be	elow ground surface. The boring	was						Groun	dwater etion	was n	ot obs	erved	during	drilling or after
	F	5-	-	back 2023	tilled with auger cuttings on Febr 3.	uary 06,						GENE	RAL N	OTES	ation a	nd ele	vation	are approximate and were
												estima	ated by	Kleinfe	elder.		to loca	are approximate and were
	Ļ											accura	acy of 1	5 feet.	in was	useu	10 1008	
SA	045																	
TUL	-815	-																
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Е IJ	F	-																
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PIT S		10-																
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52.00(NG/T																		
2300(BOR	F		1															
RLF																		
MBE	-810	-	1															
3.GLE																		
0JEC	F		-															
PR RAR)																		
LIB.	L																	
GINI	Ē.	-																
ARD																		
_2023 TAND			1			PRO		0 ·				50			0 5			BORING
aster_ LF_S						20230	0052.00	06A				RO	KING	5 LO	G B-	ğ		
int E.K.	/	-		_`														
KIf_g LATE		F	(L	E	NFELDER		WN BY:		BAG	2	5th W.	Aven	ue Wi	denin	g Reta	aining	Walls	。 B-8
FILE:			_	Bri	gnt reopie. Kight Solutions.	CHEC	CKED E	BY:	SYW			Gi T	lcreas ulsa. (e Mu: Oklah	seum oma			
gINT i gINT 7						DATE	:		3/29/2023				, .					PAGE: 1 of 1

iZhang	Date	Beg	in - E	nd:	2/06/2023	Drilling	Comp	any:	Aimri	ght Te	sting							BORING LOG B-9
. ≺	Logo	ged E	By:		B. Goben	Drill Cre	w:		P. Sc	arboro	ugh			L				
AM B	Hor.	Vert	. Dati	um:	Not Available	Drilling	Equip	ment:	Diedr	ich D-5	50		Ha	mme	[.] Туре	ə - Dr	ор: _	140 lb. Auto - 30 in.
0:46 /	Plun	ge:			-90 degrees	Drilling	Metho	d:	Solid	Flight	Auger		Ha	mme	Effic	iency	y: _	78.7%
23 10	Wea	ther:			Not Available	Explorat	ion Di	iamet	er: 6 in. (D.D.			На	mme	^r Cal.	Date		2/02/2023
31/20					FIELD EX	PLORATION	N							LA	BORA	TORY	' RESL	JLTS
PLOTTED: 03/	pproximate levation (feet)	epth (feet)	iraphical Log	Арр	Latitude: 36.17516° N Longitude: -96.01970° E roximate Ground Surface Elevation (Surface Condition: Grass	ft.): 823.0	ample umber	ample Type	ow Counts(BC)= ncorr. Blows/6 in.	ecovery NR=No Recovery)	SCS ymbol	/ater ontent (%)	ry Unit Wt. (pcf)	assing #4 (%)	assing #200 (%)	iquid Limit	lasticity Index VP=NonPlastic)	dditional Tests/ emarks
ŀ	ĀΠ	Δ	U SV/	TOP	Lithologic Description		ΰZ	ő	ΞĊ	ъ<	⊃ŵ	≤ŭ	Ō	ď.	e E	Ξ	ΞĘ	Υ Ă Υ
				TOPS				1										
-		_		High reddi	ly Weathered SANDSTONE: bro sh brown, extremely weak	own and												
-	-820	1		SANI	DSTONE : brown and reddish bro mely weak	own,	SS-1	B	C=50/5.5"	5"		14.0		100	26			
Γ				 ·		imat-lui 4						<u>GROU</u>			<u>EVEL</u>	<u>INFO</u>	RMAT	ION:
				I he t ft. be	boring was terminated at approx low ground surface. The boring	imately 4 I was						Ground	dwater etion.	was n	ot obse	erved	during	drilling or after
F	-	5-		backt	filled with auger cuttings on Feb	ruary 06,						GENE The ex	RAL No	<u>OTES:</u> on loca	ation a	nd ele	vation	are approximate and were
				2023	kfilled with auger cuttings on February 06, 3. A Handheld GPS unit was completion. GENERAL NOTES: The exploration location and elevation are ap estimated by Kleinfelder. A Handheld GPS unit was used to locate the accuracy of 15 feet.							te the exploration with an						
-	-	_										accura	icy of 1	5 feet.	iit was	uscu	10 1000	
SA																		
IN	-	_																
TER:																		
-	-815	-																
FFICE																		
0		_																
IL LO																		
T SO																		
IL LO	-	10-																
006A 3/TE8																		
D052.		_																
2023(F_BC																		
ER:																		
	-	-																
23.GI																		
7_20	-810	-																
PI																		
.NID																		
ARD																		
aster_2023 LF_STAND						PRO 2023	JECT N 0052.00	10.: 06A				BO	RING	6 LO	G B-	9		BORING
int_m E:K	ſ	-							_									
Klf_g _ATE		K	L	Eli	NFELDER	DRA	WN BY		BAG	25	5th W.	Avenu	ue Wie	dening	g Reta	aining	Walls	₅ B-9
EMPL	1			Brig	gnt People. Right Solutions.	CHE	CKED E	BY:	SYW			Gi	Icreas	e Mus	seum	-		
		-	-	/		ļ						т	ulsa ()klah	oma			







/iZhang	Date	e Beç	jin - E	ind:	2/09/2023	Drilling	Comp	any	: <u>Aimri</u>	ght Te	sting							BORING LOG B-13
37: 7	Log	ged l	Зу:		Y. Zhang	Drill Cre	ew:		H. W	lson								
AM E	Hor.	-Ver	t. Dat	um:	Not Available	Drilling	Equip	mei	nt: <u>CME</u>	-550X			Ha	mme	r Тур	e - Dr	op: _	140 lb. Auto - 30 in.
0:46	Plur	nge:			-90 degrees	Drilling	Metho	d:	Solid	Flight	Auger		Ha	mme	r Effic	cienc	y: _	77%
23 1	Wea	ather	:		Not Available	Explora	tion D	iam	eter: 6 in. (D.D.	I		Ha	mme	r Cal.	Date	: _	2/02/2023
31/20					FIELD EX	PLORATIO	N	_						LA	BORA	TORY	RESU	LTS
PLOTTED: 03/	sroximate vation (feet)	oth (feet)	phical Log	Арр	Latitude: 36.16922° N Longitude: -96.01988° E roximate Ground Surface Elevation Surface Condition: Asphalt	(ft.): 804.0	nple nber	nple Type	r Counts(BC)= orr. Blows/6 in.	overy (=No Recovery)	CS nbol	ter ntent (%)	Unit Wt. (pcf)	ssing #4 (%)	ssing #200 (%)	uid Limit	sticity Index =NonPlastic)	ittional Tests/ marks
	App Elev	Dep	Gra		Lithologic Description		San	San	Blow	Rec (NR	US(Wat Cor	Dry	Pas	Pas	Ligu	(NP	Ado Rer
				ASP	HALT: 14 inches			ł										
	-	-		FILL with dens	- Silty Clayey SAND (SC-SM): reddish brown and gray, moist, e	brown medium	SS-1		BC=10 6 6	18"	SC-SM	9.2		100	48	25	7	-
		- 5		FILL reddi	- Sandy Lean CLAY (CL): brow ish brown and gray, moist, stiff	n with	SS-2		BC=8 5 9	17"	CL	11.7		100	54	34	15	-
	- - 795	-		SILT stiff t mica	(ML): light brown with light gray o very stiff, reddish brown inclus ceous inclusions, laminated, sil	y, moist, sions, Ity texture												-
rer: Tulsa	-	10- - -		High light inclu	ly Weathered SHALE : light brov gray, extremely weak, reddish b sions, micaceous inclusions, la	wn with prown minated			BC=8 9 13	18"	ML	15.1		100	92	47	18	-
T SOIL LOG]		- - 15-		SHA	LE : gray with brown, extremely v	weak,	SS-4		BC=27 44 50/5.5"	18"		10.0		100	89	41	14	-
OJECT NUMBER: 20230052.006A _2023.GLB	- 	- - 20-		with mica The 16.5 back surfa	dark gray lenses, laminated, tra ceous inclusions boring was terminated at approx ft. below ground surface. The t filled with auger cuttings and pa ice on February 09, 2023.	ximately poring was atched at						GROL Groun <u>GENE</u> The ex estima A Han accura	INDW/ dwater etion. RAL N xplorati ted by dheld (acy of 1	ATER I was n OTES on loca Kleinfe BPS ur 5 feet.	LEVEL ot obs ation a elder. nit was	<u>INFO</u> erved and ele	RMAT during vation to loca	<u>ON:</u> drilling or after are approximate and were te the exploration with an
int_master_2023 PR(: E:KLF_STANDARD_GINT_LIBRARY	780					PRC 2023	DJECT N 30052.00	IO.: 06A				BOF	RING	LO	G B-1	13		BORING
gINT FILE: KIfg gINT TEMPLATE				E/I Brig	NFELDER ght People. Right Solutions.	DRA CHE DAT	WN BY CKED I	: 3Y:	YZ SYW 3/29/2023	2	5th W.	Aven Gi T	ue Wi ilcreas Tulsa, (dening e Mus Oklah	g Reta seum oma	aining	Walls	B-13

Date	e Beç	gin - E	nd:	2/09/2023	Drilling	Comp	any:	Aimri	ght Te	sting							BORING LOG B-14
Log	ged I	By:	-	Y. Zhang	Drill Cro	ew:		<u>H. W</u>	Ilson					_	_		
Hor.	-Ver	t. Dat	um:	Not Available	Drilling	Equip	men	t: <u>CME</u>	-550X			На	mme	r Type	e - Dr	op: _	140 lb. Auto - 30 in.
Plun	nge:		-	-90 degrees	Drilling	Metho	od:	Solid	Flight	Auger		На	mme	r Effic	cienc	y: _	77%
Wea	ather	:	-	Not Available	Explora	tion D	iame	eter: 6 in.	0.D.			Ha	mme	r Cal.	Date	: _	2/02/2023
				FIELD E	XPLORATIO	N							LA	BORA	TORY	' RESI	JLTS
vroximate vation (feet)	oth (feet)	phical Log	Appr	Latitude: 36.16949° N Longitude: -96.01988° E oximate Ground Surface Elevation Surface Condition: Asphalt	(ft.): 813.0	nple nber	nple Type	. Counts(BC)= orr. Blows/6 in.	overy =No Recovery)	CS nbol	ter ntent (%)	Unit Wt. (pcf)	sing #4 (%)	sing #200 (%)	uid Limit	sticity Index =NonPlastic)	iitional Tests/ narks
App Eley	Dep	Gra		Lithologic Description		San	San	Blow Unco	Rec (NR	USC	Wat Cor	Dry	Pas	Pas	Liqu	(NP	Add Ren
			ASPH	ALT: 12 inches			T										
	-		Highl y grayis	y Weathered SANDSTONE: li h brown, extremely weak	ght	SS-1		BC=12 19 16	12"		12.7		100	33			
-810	-						T										
	5-		SAND with g micac	STONE: yellowish brown, ver ray clay lenses, weakly ceme eous inclusions	y weak, nted, trace	- <u>SS-</u> 2·		BC=50/3"	3"								
-805	-																
000						-SS-3		BC=50/2"	2"								
	-																
	10-																
	-																
			- dark	reddish brown below 11.5'													
	-																
-800	-																
	-	<u> ····</u>				SS-4		BC=50/1.5"	2"								
-	15-	-	The b 13.5 fi backfi surfac	oring was terminated at appro t. below ground surface. The lled with auger cuttings and p æ on February 09, 2023.	oximately boring was atched at						GROL Groun comple <u>GENE</u> The ex	INDWA dwater etion. RAL No ploration	ATER I was n OTES: on loca	LEVEL ot obs	<u>. INFO</u> erved nd ele	RMAT during	<u>ION:</u> drilling or after are approximate and were
											A Han	dheld (SPS ur 5 feet	nit was	used	to loca	te the exploration with an
	-	1									400010	.5, 01 1	5 1001.				
-795	-	1															
	-	-															
-	20-																
	20-																
	-	1															
	-	-															
-790	_																
	-	1															
					PRC 2023	0JECT N 30052.0	VO.: 06A				BOF	RING	LO	G Β-΄	14		BORING
_ /		11	E //			WN BY	/ :	YZ									B-14
(k		C //	VFELDER					2!	5th W	Aven	ue Wi	denin	a Ret:	ainino	ı Wallı	
	k		E II Brig	ht People. Right Solutions.	CHE	ECKED	BY:	SYW	2	5th W.	Aven Gi	ue Wie Icreas	dening e Mu	g Reta seum	aining	Walls	







Date	e Be	gin ·	- Ene	d: <u>2/09/2023</u>		Drilling	Comp	any	: <u>Aimri</u>	ght Te	sting							В	ORING LOG	B-18
Log	ged	By:		Y. Zhang		Drill Cre	ew:		H. Wi	lson										
Hor.	-Ver	t. D	atun	n: Not Available		Drilling	Equip	mer	nt: <u>CME</u> -	550X			Ha	mme	r Type	e - Dr	op: _	140 lb.	Auto - 30 in	. <u> </u>
Plur	nge:			-90 degrees		Drilling	Metho	d:	Solid	Flight	Auger		Ha	Imme	r Effic	ciency	y: _	77%		
Wea	ather	:		Not Available		Explora	tion D	iam	eter: 6 in. ().D.			Ha	mme	r Cal.	Date	: _:	2/02/20	023	
					FIELD EXPL	LORATIO	N							LA	BORA	TORY	RESU	JLTS		
proximate evation (feet)	pth (feet)	aphical Log	-	Latitude: 36. Longitude: -96 Approximate Ground Surfa Surface Condi	.17059° N 6.01987° E ace Elevation (ft.) tion: Asphalt): 847.0	mple imber	imple Type	w Counts(BC)= corr. Blows/6 in.	covery R=No Recovery)	SCS mbol	ater intent (%)	y Unit Wt. (pcf)	issing #4 (%)	ssing #200 (%)	quid Limit	asticity Index P=NonPlastic)		ditional Tests/ :marks	
¢₩	De	ບັ		Lithologic D	escription		Sa Nu	Sa	Unc	S.S.	Sy	аS	D	Ра	Ра	Lio	₽Z.		Ad Re	
				ASPHALT: 12 inches																
-845				Highly Weathered SANI with light brown and redo weak, trace micaceous in SANDSTONE: light grayi weak, with rust mottling a nclusions, highly weathe	DSTONE: light dish brown, ext nclusions ish brown, extr and trace mica ered	gray tremely emely aceous	SS-1		BC=33 50/5"	11"		10.9		100	31					
	5-			· dark gray inclusions sta	arting at 5'		SS-2	ł	BC=50/5.5"	6"										
-840					Ū															
	10-			SANDSTONE: light grayi	ish brown to lig	ght	- <u>SS-</u> 3-		BC=50/2.5" ر	3"										
-835				orown, extremely weak, v	weathered															
	15-		· · · · · · · · · · · · · · · · · · ·				<u>_SS-4</u>		BC=50/5"	5"										
-830																				
-825	20-			The boring was terminat 20 ft. below ground surfa backfilled with auger cutt surface on February 09,	ed at approxim ace. The borin tings and patcl 2023.	nately ig was hed at	L <u>SS-5</u> -		BC=50/2.25"/	2"		GROU Groun comple <u>GENE</u> The e> estima A Han accura	INDW/ dwater etion. RAL Nr plorati ted by dheld C icy of 1	ATER I was n OTES: on loca Kleinfe GPS ur 5 feet.	<u>EVEL</u> ot obse ation a elder. nit was	INFO erved nd ele used	RMAT during vation to loca	I <u>ON:</u> drilling are app	or after proximate and exploration wit	were h an
				`		PRO 2023	JECT N 80052.0	IO.: 06A				BOF	RING	LOC	G B-′	18			BORIN	G
	×	</td <td>.E</td> <td>Bright People. Right</td> <td>DER Solutions.</td> <td>DRA CHE</td> <td>WN BY</td> <td>′: BY:</td> <td>YZ SYW</td> <td>2!</td> <td>ōth W.</td> <td>Avenı Gi T</td> <td>ue Wi Icreas ulsa, (</td> <td>dening e Mus Oklah</td> <td>g Reta seum oma</td> <td>aining</td> <td>Walls</td> <td>6</td> <td>B-18</td> <td>3</td>	.E	Bright People. Right	DER Solutions.	DRA CHE	WN BY	′: BY:	YZ SYW	2!	ōth W.	Avenı Gi T	ue Wi Icreas ulsa, (dening e Mus Oklah	g Reta seum oma	aining	Walls	6	B-18	3
						DAT	E:		3/29/2023										PAGE: 1	of 1

I∠hang	Date	e Be	gin -	End	d: <u>2/09/2023</u>	_ Drilling	g Comp	bany	/: <u>Aimri</u>	ght Te	sting							BORING LOG B-19
3Y: Y	Log	ged	By:		Y. Zhang	Drill C	rew:		H. Wi	lson				L				
	Hor.	-Ver	t. Da	atum	n: Not Available	_ Drilling	g Equip	ome	nt: <u>CME</u> -	550X			На	mme	r Type	e - Dr	ор: _	140 lb. Auto - 30 in.
	Plur	nge:			-90 degrees	Drilling	g Metho	od:	Solid	Flight	Auger		Ha	mme	r Effic	cienc	y: _	77%
	Wea	ather	:		Not Available	Explor	ation D	iam	neter: 6 in. (D.D.			На	mme	r Cal.	Date	: _	2/02/2023
					FIELD	EXPLORATION	N							LA	BORA	TORY	RESU	ILTS
	Approximate Elevation (feet)	Depth (feet)	Graphical Log		Latitude: 36.17086° N Longitude: -96.01985° Approximate Ground Surface Eleva Surface Condition: Aspl Lithologic Descriptic	l E tion (ft.): 847.0 nalt	Sample Number	Sample Type	Blow Counts(BC)= Uncorr. Blows/6 in.	Recovery (NR=No Recovery)	USCS Symbol	Water Content (%)	Dry Unit Wt. (pcf)	Passing #4 (%)	Passing #200 (%)	Liquid Limit	Plasticity Index (NP=NonPlastic)	Additional Tests/ Remarks
				4	SPHALT: 11.5 inches			I										
-	-845			• • • • • • • • • • • • • • • • • • •	tighly Weathered SANDSTONE with light brown and reddish brow veak, trace micaceous inclusion SANDSTONE: light brown with light witremely weak, reddish brown r nicaceous inclusions	i: light gray wn, extremely s ght gray, nottling, trace	SS-1		BC=28 50/5.25"	11"		8.6		100	34			-
-	-840	5-		•			SS-2		BC=50/5.5"	6"								-
-				•														-
_	-835	10-		• • •	SANDSTONE: light brown with light extremely weak, with reddish bro nterbedded throughout	ght gray, wn lenses	_ <u>SS-3</u>		BC=50/4.75"									-
_				•														-
_	-830	15-		•			- <u>SS-</u> 4		BC=50/3.5" _	4"								-
_		20-			dark reddish brown and dark g	av lenses at	- 55-5		BC=50/3 5" -	۵"								-
_	-825			2 1 2 1 2 b s	The boring was terminated at ap 20' 20,5 ft. below ground surface. T vackfilled with auger cuttings and surface on February 09, 2023.	proximately he boring was d patched at	/			<u> </u>		GROL Groun comple <u>GENE</u> The ex estima A Han accura	INDW A dwater etion. RAL Ne ploration ted by dheld C held C hey of 1	ATER I was n OTES on loca Kleinfe GPS ur 5 feet.	LEVEL ot obs ation a elder. nit was	<u>INFO</u> erved nd ele	RMAT during vation to loca	ON: drilling or after are approximate and were te the exploration with an
	/				\	PR 202	OJECT N 230052.0	NO.: 106A				BOF	RING	LO	G B-′	19		BORING
		¥	<l =</l 	.E	Bright People. Right Solution		AWN BY ECKED	r: BY:	YZ SYW	2	ōth W.	. Aven Gi T	ue Wie Icreas Julsa, (dening e Mu Oklah	g Reta seum oma	aining	y Walls	B-19
L							· L.		512312023									PAGE: 1 of 1

iZhang	Date	e Beç	jin - I	End:	2/10/2023	Drilling	Comp	any	: <u>Aimri</u>	ght Te	sting							BORING LOG B-20
3Y: Y	Log	ged I	Зу:		Y. Zhang	Drill Cre	w:		P. Sc	arboro	ugh			L				
AM E	Hor.	-Ver	t. Dat	um:	Not Available	Drilling	Equip	mei	nt: Diedri	ich D-	50		Ha	mme	r Type	e - Dr	ор: _	140 lb. Auto - 30 in.
0:47 /	Plun	nge:			-90 degrees	Drilling	Metho	d:	Solid	Flight	Auger		Ha	mme	r Effic	ciency	y: _	78.7%
23 1	Wea	ather	:		Not Available	Explorat	tion Di	iam	eter: 6 in. (D.D.			Ha	mme	r Cal.	Date		2/02/2023
31/20					FIELD EX	PLORATIO	N							LA	BORA	TORY	' RESL	ILTS
PLOTTED: 03/3	vroximate vation (feet)	oth (feet)	phical Log	Арр	Latitude: 36.17114° N Longitude: -96.01994° E oroximate Ground Surface Elevation (Surface Condition: Grass	ft.): 850.0	nple nber	nple Type	Counts(BC)= orr. Blows/6 in.	overy :=No Recovery)	CS nbol	ter itent (%)	Unit Wt. (pcf)	ising #4 (%)	sing #200 (%)	uid Limit	sticity Index =NonPlastic)	iitional Tests/ narks
	App Ele	Dep	Gra		Lithologic Description		San Nun	San	Blow Unco	Rec (NR	USC	Wat Con	Dry	Pas	Pas	Liqu	Plas (NP	Add Ren
			<u></u>	TOP	SOIL: 6 inches		SS-1		BC=2	16"		15.7		100	30			
	-	-		Silty dens	SAND (SM): light brown, moist, se, trace clay, fine roots	medium			4 7									-
	-	-		- bec	comes harder at 2.5'													-
	-845	5-		SAN	DSTONE: light gravish brown ex	tremely	-99-2	1	BC=50/3"	3"								_
	_			weak	k, weathered	aremery	00-2	ł	00-00/0									
								ł										
	-	-						ł										-
	-	-						ł										-
								ł										
	-	-																-
	-840	10-					55-3	1	BC=50/5 5"	6"								-
							00-0	7	00-00/0.0	0								
SA	-	-						ł										-
In I	-	-						ł										-
TER	_	_						ł										_
								ł										
DEFIC	-	-						ł										-
G C	-835	15-					00.4	Į	DO-50/2 5"	411								-
OIL LO				L bec	comes more coarse at 15	/	LSS-4-		LBC=50/3.5" ,									
IT SC	-	-		The	boring was terminated at approx	imately						GROU	dwater	was n	_EVEL ot obs	erved	<u>RMA I</u> during	<u>ON:</u> drilling or after
A STP	-	-	-	15.5 back	ft. below ground surface. The b filled with auger cuttings on Feb	oring was ruary 10,						comple GENE	etion. <u>RAL N</u>	OTES	_			
2.006. JG/TE	_	_		2023	3.							The exertimation	cplorati ated by	on loca Kleinfe	ation a elder.	nd ele	vation	are approximate and were
3005. 30RIN		-										A Hane accura	dheld (acy of 1	GPS ur 5 feet.	nit was	used	to loca	te the exploration with an
LF_B	-	-	1										-					
BER	-830	20-	ļ															
RUM GLB		_,																
ECT 023.(-	-	1															
RY_2	-	-																
I IBRA																		
	-	-	1															
"GI	-	-																
3 DARI																		
ster_202 =_STAN						PR0	JECT N	IO.:				BOF	RING	LO	G B-2	20		BORING
t_ma E:KLI	1			1														
If_gin \TE:		k	٢L	E/	NFELDER	DRA	WN BY	:	YZ	2	5th \//	Δυσο	۱۸/۱	donin		ainina	\M/all	B-20
E: Ki MPLA	1	~		Bri	ght People. Right Solutions.	CHE	CKED E	BY:	SYW		JUI VV.	Gi	lcreas	e Mu	seum	an in ig	vvalis	, •
TFIL							=.		3/20/2022			Т	ulsa,	Oklah	oma			
gIN N									012012020									PAGE: 1 of 1

	e Beg	gin -	End:	2/09/2023	Drilling	Comp	any:	Aimri	ght Te	sting							BORING LOG B
Log	ged	By:		Y. Zhang		ew:		H. Wi	Ison				•	_	_		
Hor.	-Ver	t. Da	tum:	Not Available	Drilling	Equip	ment:	CME-	550X			На	mme	r Тур	e - Dr	op: _	140 lb. Auto - 30 in.
Plun	nge:			-90 degrees	Drilling	Metho	d:	Solid	Flight	Auger		На	mme	r Effic	cienc	y: _	77%
Wea	ather	:		Not Available	Explora	tion Di	iamet	er: 6 in. ().D.			На	mme	r Cal.	Date	: _	2/02/2023
				FIELD I	EXPLORATIO	N							LA	BORA	TOR	RESL	JLTS
Approximate Elevation (feet)	Jepth (feet)	Sraphical Log	App	Latitude: 36.17141° N Longitude: -96.01985° E oroximate Ground Surface Elevatic Surface Condition: Aspha	on (ft.): 846.0 Ilt	Sample Number	Sample Type	llow Counts(BC)≓ Jncorr. Blows/6 in.	Recovery NR=No Recovery)	JSCS Symbol	Nater Content (%)	Dry Unit Wt. (pcf)	assing #4 (%)	^o assing #200 (%)	-iquid Limit	Plasticity Index NP=NonPlastic)	Additional Tests/ Remarks
	-	Ŭ	ASP	HALT: 12 inches		0,2	Ĩ		H)		20		4		-		~~
-845			High grayi weał	ly Weathered SANDSTONE: sh brown with reddish brown, <, trace micaceous inclusions	light extremely	SS-1	BC	C=26 50/5.75"	12"		8.4		100	23			
-840	5-		SAN weat	DSTONE : light grayish brown, <, weathered, weakly cemente	, very ed	SS-2	BO	C=37 50/1.5" _/	8"								
-835	- - - - -					- <u>SS-</u> 3-		C=50/2.75"/	3"								
-830	15-		- trac	ce water at 15'		_ <u>SS-4</u> _	B	C=50/4"	4"								
	- 20		- bec	comes lighter in color at 18'			В	C=50/3.5" /	2"								
-825		-	The 20 ft. back surfa	boring was terminated at appi below ground surface. The b filled with auger cuttings and ace on February 09, 2023.	roximately boring was patched at		_				<u>GROL</u> Groun comple <u>GENE</u> The ex estima A Hand accura	INDW A dwater etion. RAL Ne ploration ated by dheld C acy of 1	ATER I was n OTES on loca Kleinfe SPS ur 5 feet.	LEVEL ot obs ation a elder. nit was	<u>INFC</u> erved and ele	RMAT during vation to loca	I <u>ON:</u> drilling or after are approximate and w ate the exploration with a
					PRC 2023)JECT N 30052.00	IO.: 06A				BOF	RING	LO	G B-2	21		BORING
(ŀ	٢L	EI. Brig	NFELDER ght People. Right Solutions	DRAWN BY: YZ Itions. CHECKED BY: SYW SYW CHECKED BY: SYW					" B-21							

2	Date	e Beç	gin -	End:	2/10/2023	Drilling	Comp	any	r: <u>Aimri</u>	ght Te	sting							В	ORING L	_OG B-22
	Log	ged	By:		Y. Zhang	Drill Cr	ew:		P. Sc	arborc	ugh			L						
	Hor.	-Ver	t. Da	tum:	Not Available	Drilling	Equip	mei	nt: Diedr	ich D-	50		Ha	mme	r Type	e - Dr	ор: _	140 lb.	Auto - 3	30 in.
	Plur	nge:			-90 degrees	Drilling	Metho	od:	Solid	Flight	Auger		Ha	mme	r Effic	cienc	y: _	78.7%		
	Wea	ather	•		Not Available	Explora	tion D	iam	eter: 6 in.	D.D.			Ha	mme	r Cal.	Date	: _	2/02/2	023	
					FIELD EX	PLORATIC	N							LA	BORA	TOR	RESU	JLTS		
	oroximate vation (feet)	pth (feet)	tphical Log	Ар	Latitude: 36.17167° N Longitude: -96.01993° E proximate Ground Surface Elevation (Surface Condition: Grass	ft.): 849.0	nple nber	nple Type	/ Counts(BC)= orr.Blows/6 in.	covery (=No Recovery)	CS nbol	ter ntent (%)	Unit Wt. (pcf)	ssing #4 (%)	ssing #200 (%)	uid Limit	sticity Index =NonPlastic)		ditional Tests/ marke	
	App Ele	Dep	Gra		Lithologic Description		Sar	Sar	Blow	Rec NR	USU	Cor	Dry	Pas	Pas	Ligu	(NP NP		Add	
			377.	TOP	SOIL: dark brown, moist, 5 inche	es	SS-1		BC=3	16"		14.8		100	28					
_	-845			San brov	dy SILT (ML): light grayish brown vn, moist, loose IDSTONE: light grayish brown, ve	n with ery weak			3											
-		5					- <u>SS-</u> 2		<u>√BC=50/3.5"</u> ∕	4"										-
	-840	-		- silt	y texture starting at 8'															-
							- <u>SS-</u> 3'		\ <u>BC=50/2.75</u> "	3"										
_	-835	15-		- fer	rous inclusions and rust staining	at 15',	-SS-4		BC=50/4" /	4"	-	9.8		100	36					-
-	-830			becc inclu	omes dark gray and dark reddish usions below 16'	brown														
-		20-					- <u>SS-</u> 5		\ <mark>BC=50/3.5"</mark> ∕	4"										-
-	-825	- 25-		- - - ligi	ht gray at 25'	,			\BC=50/2.5" /	3"										
-	-820	The boring was terminated at approxim 25 ft. below ground surface. The borin backfilled with auger cuttings on Febru 2023.]				-	GROL Groun compl <u>GENE</u> The ex estima A Han accura	<u>JNDW</u> dwater etion. <u>RAL N</u> xplorati ated by dheld (acy of 1	ATER I was n OTES: on loca Kleinfe GPS ur 5 feet.	LEVEL ot obs ation a elder. nit was	<u>INFO</u> erved and ele	RMAT during vation to loca	<u>ION:</u> drilling are app ate the e	or after proximate exploratio	and were n with an
	/						ROJECT NO.: 230052.006A					BO	RING	IG LOG B-22					BO	RING
		KLEINFELDER Bright People. Right Solutions.					AWN BY ECKED I	′: BY:	YZ SYW	2	5th W.	. Aven Gi T	ue Wi ilcreas ulsa,	dening e Mus Oklah	g Reta seum oma	aining	y Walls	6	B	-22
							с.		312912023	PAGE: 1 of 1							1 of 1			

iZhang	Date	e Be	gin - I	End:	2/09/2023	Drilling	Compa	any	r: <u>Aimri</u>	ght Te	sting							в	DRING L	OG B-23	
Υ: Υi	Log	ged	By:		Y. Zhang	Drill Cre	ew:		H. Wi	lson				L							
AM B	Hor	Ver	t. Dat	um:	Not Available	Drilling	Equip	nei	nt: <u>CME</u> -	550X			Ha	mme	r Type	e - Dr	op: _	140 lb.	Auto - 3	0 in.	
0:48 /	Plur	nge:			-90 degrees	Drilling	Metho	d:	Solid	Flight	Auger		Ha	mme	r Effic	ciency	/: _	77%			
23 1(Wea	ather	:		Not Available	Explora	tion Di	am	eter: 6 in. (D.D.			Ha	Imme	r Cal.	Date	: _	2/02/20)23		
31/20					FIELD E	XPLORATIO	N							LA	BORA	TORY	RESL	JLTS			
PLOTTED: 03/3	pproximate evation (feet)	spth (feet)	aphical Log	Apj	Latitude: 36.17196° N Longitude: -96.01985° E proximate Ground Surface Elevation Surface Condition: Asphalt	(ft.): 836.0	ample umber	ample Type	w Counts(BC)= corr. Blows/6 in.	scovery R=No Recovery)	SCS mbol	ater ontent (%)	y Unit Wt. (pcf)	assing #4 (%)	assing #200 (%)	quid Limit	asticity Index P=NonPlastic)		lditional Tests/ emarks		
	ЧР Ш	Ď	ō		Lithologic Description		Sa Nu	Sa	CBIO	δZ	sy Sy	Χö	D	Ра	Ра	Ľ	₽Z		Ad Re		
	005		1111:	ASP	HALT: 9 inches		00.4	Ł	DO-50/5"	C "	-			100	22						
	- 835			light - beo	gray to reddish brown, extreme comes light grayish brown with ling and ferrous inclusions at 2'	rown with Iy weak rust	_55-1_		_ <u>BC=50/5</u>			1.1		100	22						
	-																				
	-	5-					SS-2	ŀ	BC=26 50/5"	11"											
	830 -							ł]										
	-							ł													
	-							ł													
	-	10-					<u>-SS-3</u> -	ł	\BC=50/1.5" /	2"											
	-825							ł													
	-							ł													
	_			- beo	comes gray with light brown at ?	13'		ł													
	-	15-		6 11 T	STONE light brown with growt	0.010000	SS-4		BC=46 50/2"	6"		9.9		100	59						
	820 -		× × × × × × × × × × × × × × × × × × ×	with	reddish brown, extremely weak	o orange															
OIL LOG]	-		× × × × × × × ×	- beo trace	comes brown with reddish brow e micaceous inclusion at 18'	n with															
T PIT S	_	20-					-SS-5-	ł	ъс=50/3" л	3"	-										
NG/TES	-815							ł													
^c _BORI	_							ł													
[KLF	-							ł													
23.GLB	_	25-					SS-6	ł	BC=50/1.5" /	2"											
Υ_202	-810		-	The	boring was terminated at appro	ximately	ٽ				J	GROL	INDW A			INFO	RMAT	ION:	or offer-		
3RAR	_		4	25 ft back	. below ground surface. The bo filled with auger cuttings and pa	oring was atched at						comple	etion.	was n		eived	uunng	unning	u aller		
IT_LIE	_		4	surfa	ace on February 09, 2023.							The extinc	cplorati	on loca	ation a	nd ele	vation	are app	roximate	and were	
RD_GIN	_		-									A Han accura	dheld (acy of 1	GPS ur 5 feet.	nit was	used	to loca	ate the e	xploratior	n with an	
F_STANDA				<u> </u>		PROJECT NO.:						BOR	RING	LOC	og B-23				BOF	RING	
E:KLI	1	,	~ 1			20230052.006A													F	00	
PLATE	ĺ	r	۲L	E I . Bri	INFELDER aht People. Right Solutions.					YZ 25th W. Avenue Widening Retaining Walls					s	B-	-23				
T TEM			-				CHECKED BY: SYW				W Gilcrease Museum Tulsa, Oklahoma										
gIN							312912023	3 PAGE: 1						1 of 1							

Lipsgel By: Y. Zhang Drill Crew: P. Schotzough Hor. Vert. Datum: Addialde Drilling Equipment: Dodding 200 Hor. Vert. Datum: Addialde Drilling Method: Solid Flight Auger Westher: Not Available Exploration Diameter 6 in. 0.0. Harmer Efficiency: 78.7% Harmer Vert. Datum: FELD EXPLORATION Exploration Diameter 6 in. 0.0. Harmer Call. Date: 2022/223 Vesther: Not Available FELD EXPLORATION Exploration Diameter 6 in. 0.0. Harmer Call. Date: 2022/223 Vesther: Not Available FELD EXPLORATION Exploration Diameter 6 in. 0.0. Harmer Call. Date: 2022/223 Vesther: Not Available FELD EXPLORATION Exploration Diameter 6 in. 0.0. Harmer Efficiency: 78.7% Age of the structure of the stru	Date B	Beg	in - I	End:	2/10/2023	Drilling	Comp	any	: <u>Aimri</u>	ght Te	sting							BORING LOG B-2
Inter-Ver. Datum: No.4 Available Drilling Keipurger: Baitmer Type - 100 B. AQD Punge:	Logged	d E	By:		Y. Zhang	Drill Cre	ew:		P. Sc	arboro	ugh			L				
Plunge: _90 degrees Drilling Method: Solid Flight Auger Hammer Efficiency: 78.7% Weather: Not Available PELD EXPLORATION Hammer Cal. bits: 202/2023 Image: Solid Flight Auger FELD EXPLORATION LABORATION PRESULTS LABORATION PRESULTS Image: Solid Flight Auger Image: Solid Flight Auger Hammer Cal. bits: 202/2023 Image: Solid Flight Auger FELD EXPLORATION LABORATION PRESULTS LABORATION PRESULTS Image: Solid Flight Auger Image: Solid Flight Auger Hammer Cal. bits: 202/2023 Image: Solid Flight Auger Image: Solid Flight Auger Hammer Cal. bits: 202/2023 Image: Solid Flight Auger Image: Solid Flight Auger Hammer Cal. bits: 202/2023 Image: Solid Flight Auger Image: Solid Flight Auger Hammer Cal. bits: 202/2023 Image: Solid Flight Auger Image: Solid Flight Auger Hammer Cal. bits: 202/2023 Image: Solid Flight Auger Image: Solid Flight Auger Hammer Cal. bits: 202/2023 Image: Solid Flight Auger Image: Solid Flight Auger Hammer Cal. bits: 202/2023 Image: Solid Flight Auger Image: Solid Flight Auger Hammer Cal. bits: 202/2023 Image: Solid Flight Auger Image: Solid Flight Auger Hammer Cal. bits	HorVe	/ert	. Dat	tum:	Not Available	Drilling	Equip	mer	nt: Diedri	ch D-	50		Ha	mme	r Тур	e - Dr	ор: _	140 lb. Auto - 30 in.
Weather: Not Available Exploration Damater; 6 in . O.D. Hammer Cal. Data: 2022023 9 9 9 1	Plunge	e:			-90 degrees	Drilling	Metho	d:	Solid	Flight	Auger		Ha	mme	r Effic	ciency	y: _	78.7%
FEL DEPLOYATION LADORATION LADORATION LADIRAC SET 1721 % Lating de St 1721 % St 1051 %	Weath	ner:		1	Not Available	Exploration	tion D	iam	eter: 6 in. (D.D.	1		Ha	mme	r Cal.	Date	: _	2/02/2023
and output is an analysis of the second s					FIELD EX	XPLORATIO	N							LA	BORA	TORY	RESU	JLTS
201 3 3 2 3 25 2 2 1 3 123 100 22 1 100 22 1 100 22 100 123 100 <td>oroximate vation (feet) oth (feet)</td> <td>orn (reet)</td> <td>ıphical Log</td> <td>А</td> <td>Latitude: 36.17213° N Longitude: -96.01996° E pproximate Ground Surface Elevation Surface Condition: Grass</td> <td>(ft.): 833.0</td> <td>nple nber</td> <td>nple Type</td> <td>r Counts(BC)= brr. Blows/6 in.</td> <td>overy (=No Recovery)</td> <td>CS nbol</td> <td>ter ntent (%)</td> <td>Unit Wt. (pcf)</td> <td>ssing #4 (%)</td> <td>ssing #200 (%)</td> <td>uid Limit</td> <td>sticity Index =NonPlastic)</td> <td>ilitional Tests/ marks</td>	oroximate vation (feet) oth (feet)	orn (reet)	ıphical Log	А	Latitude: 36.17213° N Longitude: -96.01996° E pproximate Ground Surface Elevation Surface Condition: Grass	(ft.): 833.0	nple nber	nple Type	r Counts(BC)= brr. Blows/6 in.	overy (=No Recovery)	CS nbol	ter ntent (%)	Unit Wt. (pcf)	ssing #4 (%)	ssing #200 (%)	uid Limit	sticity Index =NonPlastic)	ilitional Tests/ marks
-20 TOPSOL: 3 inches BS-1 00-2 10* 12.3 100 22 -800	Ele Der	nep	Gra		Lithologic Description		San	San	Blow Unco	Rec (NR	USC	Wat Cor	Dry	Pas	Pas	Liqu	Plas (NP	Add Ren
				ТО	PSOIL: 3 inches		SS-1	Π	BC=2	16"		12.3		100	22			
SANDTONE: light gray with light brown, externely weak, weathered, weakly comented SS-2 BC-50/5 5' 	-830			bro	ty SAND (SM): brown to light gra wn with orange, moist, medium (yish dense			6									
-825 -810 -810	Ę	- 5		SA ext	NDSTONE: light gray with light b remely weak, weathered, weakly	rown, cemented	<u></u>		BC=50/5"	5"								
10 SLISTONE: light grayish brown, extremely weak, weathered, weakly ocemented, ferrous inclusions, rust mottling SS-3 BC=503.5", 4" 160 15- 15- 15- 17- 15- 15- 15- 1815 15- 15- 15- 20- 15- 15- 15- 1815 15- 15- 15- 20- 15- 15- 15- 20- 15- 15- 15- 20- 15- 15- 15- 20- 15- 15- 15- 20- 15- 15- 15- 20- 15- 15- 15- 20- 15- 15- 15- 20- 15- 15- 15- 20- 15- 15- 15- 20- 15- 15- 15- 300 15- 15- 15- 3010 15- 15- 15- 3010 15- 15- 15- 3010 15- 15- 15- 3010 15- 15- 15- 3010 15- 15- 15- 3010 15- 15- 15-	825	-																
15	-820	-		SIL we inc	. TSTONE : light grayish brown, exak, weathered, weakly cemented lusions, rust mottling	ktremely I, ferrous	- <u>5</u> S-3-	·····	-BC=50/3.5" ر	4"								
815 SS-5 BC=50/2.5° 3° The boring was terminated at approximately 20 ft. below ground surface. The boring was backfilled with auger cuttings on February 10, 2023. SS-5 BC=50/2.5° 3° 810 GROUNDWATER LEVEL INFORMATION: Groundwater was not observed during drilling or afte completion. GENERAL NOTES: The exploration location and elevation are approxima estimated by Kleinfeider. A Handheld GPS unit was used to locate the explora accuracy of 15 feet. 810 PROJECT NO.: 20230052.006A BORING LOG B-24 B PROJECT NO.: 20230052.006A DRAWN BY: YZ 25th. W. Auguing Widening Dataining Male	15	- 15— -					- <u>SS-4</u> -		ъвс=50/2.5" у	3"								
Bornewick The boring was terminated at approximately 20 ft. below ground surface. The boring was backfilled with auger cuttings on February 10, 2023. GROUNDWATER LEVEL INFORMATION: Groundwater was not observed during drilling or after completion. GENERAL NOTES: The exploration location and elevation are approximated by Kleinfelder. A Handheld GPS unit was used to locate the explora accuracy of 15 feet. *810 PROJECT NO.: 20230052.006A PROJECT NO.: 20230052.006A BORING LOG B-24	-815 20	- - 20-					-55-5-		BC=50/2.5" r			- 81-		-100-	- 16 -			
PROJECT NO.: BORING LOG B-24 CRAWN BY: YZ	·810	-		The 20 bao 202	e boring was terminated at appro ft. below ground surface. The bc ckfilled with auger cuttings on Fe 23.	oximately oring was bruary 10,	35-3				I	GROL Groun comple <u>GENE</u> The ex estima A Han accura	INDWA dwater etion. RAL Ne ploration ploration ted by dheld C acy of 1	ATER I was n OTES: on loca Kleinfe PPS ur 5 feet.	LEVEL ot obs	<u>INFO</u> erved nd ele	RMAT during vation to loca	<u>ION:</u> drilling or after are approximate and wer ate the exploration with ar
KLEINFELDER DRAWN BY: YZ 25th W/ Avenue W/idening Detaining M/s/la	((\ \	PROJECT NO.: BORIN 20230052.006A						RING	LOC	G B-2	24		BORING	
Bright People. Right Solutions. CHECKED BY: SYW DATE: 3/29/2023		K	(L		INFELDER right People. Right Solutions.	CHECKED BY: SYW					5th W.	Aven Gi T	ue Wie Icreas ulsa, (dening e Mus Oklah	g Reta seum oma	aining	Walls	s B-24

		Beč	jin - E	End:	2/09/2023	Drilling Company: Aimright Testing Drill Crew: H. Wilson Drilling Equipment: CME-550X												BORING LOG B-25
	Logo	ged I	Зу:		Y. Zhang	Drill Cre	ew:		<u>H.</u> W	ilson								
	Hor.	-Ver	t. Dat	um:	Not Available	Drilling	Equip	mer	nt: <u>CME</u>	-550X			Ha	mme	r Тур	e - Dr	op: _	140 lb. Auto - 30 in.
	Plun	ge:			-90 degrees	Drilling	Metho	od:	Solid	Flight	Auger		Ha	mme	r Effic	cienc	у: _	77%
	Wea	ther			Not Available	Explora	tion D	iam	eter: 6 in.	0.D.			Ha	mme	r Cal.	Date	: _	2/02/2023
					FIELD E>	(PLORATIO	N							LA	BORA	TOR	RESL	JLTS
brovimate	proximate vation (feet)	pth (feet)	aphical Log	Арр	Latitude: 36.17252° N Longitude: -96.01985° E proximate Ground Surface Elevation Surface Condition: Asphalt	(ft.): 813.0	mple	mple Type	v Counts(BC)= orr. Blows/6 in.	covery R=No Recovery)	iCS mbol	ater ntent (%)	/ Unit Wt. (pcf)	ssing #4 (%)	ssing #200 (%)	uid Limit	sticity Index >=NonPlastic)	ditional Tests/ marks
<	Ele Ele	De	ũ		Lithologic Description		Sa	Sa	Unc	(NF	US Syi	So So	D	Ра	Ъа	Liq	R R	Ad
				ASP	HALT: 9 inches			I										
		-	2009	AGG	REGATE BASE: 3 inches		SS-1		BC=15	14"		13.2		100	40			
	-810	-		Silty and poss	SAND (SM): reddish brown witl gray, moist, medium dense, trad ible fill	h brown ce clay,			11 9									
		- 5—		SAN	DSTONE: light brown with gray,		- <u>SS-2</u> -		BC=50/2"	2"								
		-		extre	mely weak, weathered, weakly	cemented												
	805	-																
		-																
		10-						N	BC=50/3"	3"								
-	-800	-		The 10.5 back surfa	boring was terminated at appro ft. below ground surface. The l filled with auger cuttings and pa ace on February 09, 2023.	ximately boring was atched at						GROL Groun comple <u>GENE</u> The ey estima A Han accura	INDW/ dwater etion. RAL N kplorati ated by dheld (acy of 1	ATER I was n OTES on loca Kleinfe GPS ur 5 feet.	LEVEL oot obs ation a elder. nit was	<u>INFC</u> erved nd ele	RMAT during vation to loca	I <u>ON:</u> drilling or after are approximate and were te the exploration with an
	-795	15— - -																
-						PROJECT NO.: BORING LOG B-25							BORING					
	(×	<l< td=""><td>EI. Bri</td><td>NFELDER ight People. Right Solutions.</td><td>DRA CHE</td><td>WN BY CKED I</td><td>′: BY:</td><td>YZ SYW 3/29/2023</td><td>25</td><td>5th W.</td><td colspan="3">W. Avenue Wide Gilcrease Tulsa, O</td><td>g Reta seum oma</td><td>aining</td><td>B-25</td></l<>	EI. Bri	NFELDER ight People. Right Solutions.	DRA CHE	WN BY CKED I	′: BY:	YZ SYW 3/29/2023	25	5th W.	W. Avenue Wide Gilcrease Tulsa, O			g Reta seum oma	aining	B-25	

Da	te Be	əgin	- Ei	nd: 2/10/2023	Drilling	Comp	an	y: Aimr	ight Te	sting							BORING LOG B-26
	gged	I By:		Y. Zhang	Drill Cre	ew:		<u>P. So</u>	carboro	ugh			•	_	_		
Ho	rVe	ert. D	atu	m: Not Available	Drilling	Equip	me	ent: Died	rich D-	50		Hai	mme	r Typ	e - Dr	op: _	140 lb. Auto - 30 in.
Plu	inge			-90 degrees	Drilling	Metho	od:	Solid	Flight	Auger		Hai	mme	r Effic	cienc	y: _	78.7%
We	eathe	er:	-	Not Available	Explora	tion D	ian	neter: 6 in.	O.D.	r – –		Hai	mme	r Cal.	Date	: _	2/02/2023
			_	FIELD E	EXPLORATIO	N T	-	1					LA	BORA	TOR)	/ RESL	JLTS
pproximate levation (feet)	epth (feet)	ranhical Lod		Latitude: 36.17278° N Longitude: -96.01991° E Approximate Ground Surface Elevatio Surface Condition: Bare Earth an	n (ft.): 812.0 d Grass	ample umber	ample Tvpe	ow Counts(BC)= ncorr. Blows/6 in.	ecovery JR=No Recovery)	SCS ymbol	/ater ontent (%)	ry Unit Wt. (pcf)	assing #4 (%)	assing #200 (%)	quid Limit	lasticity Index VP=NonPlastic)	dditional Tests/ emarks
ΑШ	Δ	U SV)	Lithologic Description	E in ch	ΰZ	ŝ	<u> 話</u> 5	ĨŽ <	⊃ú	≤ Ŭ 12.0	ā	100	42		ΞĽ	Ϋ́Ϋ́
		\otimes	\mathfrak{A}	paver stone	.5-incn	35-1	N	BC=15 4	16"		13.0		100	43			
				FILL - Silty SAND (SM): light brown loose, with gray clay and trace san gravel	n, moist, dstone			3		-							
				Sandy SILT (ML): light brown, moi very loose to loose	st to wet,		ł										
- - - ⊻	⁷ 5			boomoo watat 5' traco alay su	t mottling	66.2			10"		21.7		100	52			-
				- becomes wet at 5, trace clay, rus	a mouning	33-2		WOH WOH	18		21.7		100	55			
F		-						WOH									
							1	,		-							
-805							ł										
							}										
[ł										
L							ł										
							ł										
-	10			Sandy SILT (ML): light brown with	light grov			PC-2	10"	-	21.3		100	55			
				and reddish brown, wet, medium s	tiff	33-3	ľ	BC=3	18		21.3		100	55			
-		-//						4									
-800		-		The boring was terminated at appr	oximately					∇	GROL	JNDWA	TER		. INFO	RMAT	ION: mately 5 ft, below ground
				11.5 ft. below ground surface. The backfilled with auger cuttings on Fe	e boring was ebruary 10,					=	surfac	e during	drilli	ng.	u al a	ppioxii	nately 5 ft. below ground
-		-		2023.							The ex	xploratic	n loc	<u>:</u> ation a	nd ele	vation	are approximate and were
											estima A Han	ated by ł dheld G	leinfo	elder. nit was	used	to loca	te the exploration with an
-											accura	acy of 15	5 feet.				
_	15																
	10																
-																	
-795		_															
-		-															
-		-															
					DPC												BORING
					2023	,J⊑CTN 30052.0	۷U.: 06A		1		BOI	RING	LO	G B-2	26		
	1					-			1								
		K		EINFELDER		WN BY	' :	YZ	2	5th \//	Δνοσ		lonin	a Rot	aining	1///14	B-26
	1			Bright People. Right Solutions	CHE	CKED I	BY:	SYW		JUT VV.	G	ilcrease	e Mu	seum	annng	y vv alls	
		1	/	1		ī.		3/20/2022	1		Т	ulsa, C	Oklah	ioma			
					DATE: 3/29/2023										PAGE: 1 of 1		



Zhang	Date	e Beg	in - E	nd:	2/06/2023	Drilling	Comp	any:	Aimr	ight Te	sting							BORING LOG B	-28
Υ: ΥI	Log	ged E	By:		B. Goben	Drill Cre	w:		P. So	arboro	ugh			L					
AM E	Hor.	-Vert	. Dat	um:	Not Available	Drilling	Equip	ment	: Died	rich D-	50		На	mme	r Typ	e - Dr	op: _	140 lb. Auto - 30 in.	
0:48	Plun	ige:			-90 degrees	Drilling	Metho	d:	Solid	Flight	Auger		Ha	mme	r Effic	cienc	y: _	78.7%	
023 1	Wea	ther			Not Available	Explorat	ion D	iame	ter: 6 in.	O.D.	1		Ha	mme	r Cal.	Date	: _	2/02/2023	
31/20					FIELD EX	PLORATION	۱ 							LA	BORA		(RESI	JLTS	
PLOTTED: 03/	proximate vation (feet)	pth (feet)	aphical Log	Арр	Latitude: 36.17329° N Longitude: -96.01990° E proximate Ground Surface Elevation (Surface Condition: Grass	(ft.): 827.0	mple mber	mple Type	v Counts(BC)= orr. Blows/6 in.	covery R=No Recovery)	CS mbol	ater ntent (%)	r Unit Wt. (pcf)	ssing #4 (%)	ssing #200 (%)	uid Limit	sticity Index >=NonPlastic)	ditional Tests/ marks	
	Apl Ele	De	Gra		Lithologic Description		Sal Nu	Sai	Blov	(NF Rec	US Syi	Co Co	Dry	Pa	Pa	Liq	Pla NF	Ad	
			<u>717</u>	TOP	SOIL: 6 inches														
	- 825	-		Silty reddi	SAND (SM): light brownish gray sh brown, moist, medium dense	y and e													-
	_	_						ł											-
	-	-	XXXXX	High brow	ly Weathered SILTSTONE : ligh nish gray, extremely weak	t	SS-1	F	3C=10 12 16	18"		12.5		100	56				-
	-																		-
	-820	_	$\overset{\times\times\times\times\times\times\times\times}{\times$																_
	-	-	$\overset{\times}{\times}{\times}\overset{\times}$				SS-2		3C=26	16"									-
R: TULSA	_	10-	XX	SAN	DSTONE : light brownish gray, e:	xtremely			50/4"										_
FICE FILTE	_	_																	_
IL LOG]	-815	-																	-
6A 'EST PIT SO	_	-					SS-3		3C=50/5.25'	5"									
ECT NUMBER: 20230052.00.)23.GLBKLF_BORING/T	- - 	- 15		The I 14 ft. back 2023	boring was terminated at appro- below ground surface. The boi filled with auger cuttings on Feb	kimately ring was oruary 06,		_				<u>GROL</u> Groun compl <u>GENE</u> The ex estima A Han accura	INDWA dwater etion. RAL N plorati ated by dheld (acy of 1	ATER I was n OTES on loca Kleinfe SPS ur 5 feet.	LEVEL ot obs ation a elder. nit was	<u>INFC</u> erved and ele	RMAT during vation to loca	ION: drilling or after are approximate and we ate the exploration with a	ere an
PROJE ARD_GINT_LIBRARY_20	-	-																	
naster_2023 KLF_STAND.						PRO. 2023	JECT N 0052.0	IO.: 06A				BO	RING	LO	G B-2	28		BORING	
T FILE: KIf_gint_r F TEMPLATE: E:I		×	(L)	EI Brig	NFELDER ght People. Right Solutions.	DRA CHE	DRAWN BY: BAG CHECKED BY: SYW					25th W. Avenue Wid Gilcrease Tulsa, C				nue Widening Retaining Walls Silcrease Museum Tulsa, Oklahoma			
gIN'									512912023									PAGE: 1 of	1



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LABORATORY TESTING PROGRAM

Laboratory tests were performed on select, representative samples to evaluate pertinent engineering properties of these materials. We directed our laboratory testing program primarily toward classifying the subsurface materials and measuring index values of the on-site materials. Laboratory tests were performed in general accordance with applicable standards. The results of the laboratory tests are presented on the respective boring logs. The laboratory testing program consisted of the following:

- Moisture Content, AASHTO T 265, Standard Method of Test for Laboratory Determination of Moisture Content of Soils.
- Soil Classification:
 - AASHTO T 87, Standard Method of Test for Dry preparation of Disturbed Soil and Soil Aggregate Samples for Test.
 - AASHTO T 88, Standard Method of Test for Particle Size Analysis of Soils.
 - AASHTO T 89, Standard Method of Test for Determining the Liquid Limit of Soils.
 - AASHTO T 90, Standard Method of Test for Determining the Plastic Limit and Plasticity Index of Soils.
- Visual Classification, ASTM D2488, Standard Practice for Description and Identification of Soils (Visual-Manual Procedure).

	Depth (ft.)	Sample No.	Sample Description	USCS	AASHTO	OKLAHOMA SOIL INDEX (OSI)	Water Content (%)	Atterberg Limits			Sieve Analysis (%)				
Exploration ID								Liquid Limits	Plastic Limits	Plasticity Index	Passing #4	Passing #10	Passing #40	Passing #100	Passing #200
B-1	3.5 - 5.0	SS-1			A-2-4		11.1				100	100	100	100	27
B-2	3.5 - 5.0	SS-1]	A-4		11.1				100	100	91		43
В-3	3.0 - 4.5	SS-1]	A-4		11.1				100	100	42		39
B-4	3.5 - 5.0	SS-1]	A-4		10.5				100	100	89		45
B-5	3.5 - 5.0	SS-1]	A-4		14.1				100	100	96		54
B-6	3.5 - 5.0	SS-1]	A-4		14.4				100	100	93		50
B-7	3.5 - 5.0	SS-1			A-4		20.9				100	100	95		55
B-8	3.5 - 5.0	SS-1		1	A-2-4		9.4				100	100	77		21
В-9	3.5 - 5.0	SS-1		1	A-2-4		14.0				100	100	96		26
B-10	3.5 - 5.0	SS-1		1	A-2-4		22.4				100	100	95		35
B-11	3.5 - 5.0	SS-1		1	A-4		12.1				100	100	90		43
B-12	3.5 - 5.0	SS-1		1	A-4		11.4				100	100	94		38
B-13	1.16 - 2.6	SS-1	SILTY, CLAYEY SAND	SC-SM	A-4		9.2	25	18	7	100	100	79		48
B-13	5.0 - 6.5	SS-2	SANDY LEAN CLAY	CL	A-6		11.7	34	19	15	100	100	79		54
B-13	10.0 - 11.5	SS-3	SILT	ML	A-7-6		15.1	47	29	18	100	100	97		92
B-13	15.0 - 15.5	SS-4	SILT	ML	A-7-6		10.0	41	27	14	100	100	96		89
B-14	1.0 - 2.5	SS-1		1	A-2-4		12.7				100	100	98		33
B-15	1.0 - 2.5	SS-1		1	A-4		11.8				100	100	96		44
B-15	5.0 - 5.5	SS-2		1	A-2-4		8.2				100	100	95		33
B-15	10.0 - 10.5	SS-3		1			9.8								
B-15	20.0 - 20.5	SS-5		1	A-2-4						100	100	98		35
B-16	1.0 - 2.0	SS-1		1	A-4		12.2				100	100	98		37
B-17	1.0 - 2.0	SS-1		1	A-2-4		10.7				100	100	99		30
B-17	5.0 - 6.0	SS-2			A-4						100	100	99		43
B-17	10.0 - 10.5	SS-3					10.1								•••••
B-18	1.0 - 2.0	SS-1			A-2-4		10.9				100	100	100	100	31
B-19	1.0 - 2.0	SS-1		1	A-2-4		8.6				100	100	100	100	34
B-20	0.0 - 1.5	SS-1]	A-2-4		15.7				100	100	98		30

	PROJECT NO.: 20230052.006A		LABORATORY TEST RESULT SUMMARY	TABLE		
<i>KLEINFELDER</i>	DRAWN BY:	BAG	25th W. Avenue Widening Retaining Walls	B-1		
Bright People. Right Solutions.	CHECKED BY:	SYW	Gilcrease Museum Tulsa, Oklahoma			
	DATE:	2/10/2023				

Refer to the Geotechnical Evaluation Report or the supplemental plates for the method used for the testing performed above. NP = Nonplastic NA = Not Available

	Depth (ft.)	Sample No.	Sample Description	USCS	AASHTO	OKLAHOMA SOIL INDEX (OSI)	Water Content (%)	Atterberg Limits			Sieve Analysis (%)				
Exploration ID								Liquid Limits	Plastic Limits	Plasticity Index	Passing #4	Passing #10	Passing #40	Passing #100	Passing #200
B-21	1.5 - 2.5	SS-1			A-2-4		8.4				100	100	94		23
B-22	0.0 - 1.5	SS-1			A-2-4		14.8				100	100	97		28
B-22	15.0 - 15.5	SS-4			A-4		9.8				100	100	96		36
B-23	0.75 - 1.6	SS-1		1	A-2-4		7.7				100	100	98		22
B-23	15.0 - 16.0	SS-4			A-4		9.9				100	100	85		59
B-24	0.0 - 1.16	SS-1		1	A-2-4		12.3				100	100	95		22
B-24	20.0 - 20.5	SS-5		1	A-2-4		8.1				100	100	84		16
B-25	0.75 - 1.16	SS-1			A-4		13.2				100	100	95		40
B-26	0.0 - 1.5	SS-1			A-4		13.0				100	100	93		43
B-26	5.0 - 6.5	SS-2			A-4		21.7				100	100	99		53
B-26	10.0 - 11.5	SS-3		1	A-4		21.3				100	100	97		55
B-27	3.5 - 5.0	SS-1			A-4		13.9				100	100	98		72
B-28	3.5 - 5.0	SS-1		1	A-4		12.5				100	100	92		56
B-29	3.5 - 4.0	SS-1			A-4		10.9				100	100	98		68
B-29	8.5 - 9.5	SS-2			A-4		12.0				100	100	97		78
B-30	3.5 - 4.0	SS-1			A-2-4		8.5				100	100	96		27
B-31	3.5 - 5.0	SS-1			A-4		14.5				100	100	96		74
B-32	3.5 - 5.0	SS-1			A-4		12.1				100	100	95		44
B-33	3.5 - 5.0	SS-1			A-4		8.2				100	100	95		75
B-34	3.5 - 5.0	SS-1	SILT WITH SAND	ML	A-4		13.5	30	23	7	100	100	95		76
B-35	3.5 - 5.0	SS-1]	A-4	[16.8				100	100	96		61
B-36	3.5 - 5.0	SS-1		1	A-4	[· · · · · · · ·	14.7			1	100	100	94		75

\bigcap	PROJECT NO.: 20230052.006A		LABORATORY TEST RESULT SUMMARY	TABLE		
(KLEINFELDER	DRAWN BY:	BAG	25th W. Avenue Widening Retaining Walls	B-2		
Bright People. Right Solutions.	CHECKED BY:	SYW	Gilcrease Museum Tulsa, Oklahoma			
	DATE:	2/10/2023	,			

Refer to the Geotechnical Evaluation Report or the supplemental plates for the method used for the testing performed above. NP = Nonplastic NA = Not Available



Important Information about This Geotechnical-Engineering Report

Subsurface problems are a principal cause of construction delays, cost overruns, claims, and disputes.

While you cannot eliminate all such risks, you can manage them. The following information is provided to help.

The Geoprofessional Business Association (GBA) has prepared this advisory to help you - assumedly a client representative - interpret and apply this geotechnical-engineering report as effectively as possible. In that way, you can benefit from a lowered exposure to problems associated with subsurface conditions at project sites and development of them that, for decades, have been a principal cause of construction delays, cost overruns, claims, and disputes. If you have questions or want more information about any of the issues discussed herein, contact your GBA-member geotechnical engineer. Active engagement in GBA exposes geotechnical engineers to a wide array of risk-confrontation techniques that can be of genuine benefit for everyone involved with a construction project.

Understand the Geotechnical-Engineering Services Provided for this Report

Geotechnical-engineering services typically include the planning, collection, interpretation, and analysis of exploratory data from widely spaced borings and/or test pits. Field data are combined with results from laboratory tests of soil and rock samples obtained from field exploration (if applicable), observations made during site reconnaissance, and historical information to form one or more models of the expected subsurface conditions beneath the site. Local geology and alterations of the site surface and subsurface by previous and proposed construction are also important considerations. Geotechnical engineers apply their engineering training, experience, and judgment to adapt the requirements of the prospective project to the subsurface model(s). Estimates are made of the subsurface conditions that will likely be exposed during construction as well as the expected performance of foundations and other structures being planned and/or affected by construction activities.

The culmination of these geotechnical-engineering services is typically a geotechnical-engineering report providing the data obtained, a discussion of the subsurface model(s), the engineering and geologic engineering assessments and analyses made, and the recommendations developed to satisfy the given requirements of the project. These reports may be titled investigations, explorations, studies, assessments, or evaluations. Regardless of the title used, the geotechnical-engineering report is an engineering interpretation of the subsurface conditions within the context of the project and does not represent a close examination, systematic inquiry, or thorough investigation of all site and subsurface conditions.

Geotechnical-Engineering Services are Performed for Specific Purposes, Persons, and Projects, and At Specific Times

Geotechnical engineers structure their services to meet the specific needs, goals, and risk management preferences of their clients. A geotechnical-engineering study conducted for a given civil engineer will <u>not</u> likely meet the needs of a civil-works constructor or even a different civil engineer. Because each geotechnical-engineering study is unique, each geotechnical-engineering report is unique, prepared *solely* for the client.

Likewise, geotechnical-engineering services are performed for a specific project and purpose. For example, it is unlikely that a geotechnical-engineering study for a refrigerated warehouse will be the same as one prepared for a parking garage; and a few borings drilled during a preliminary study to evaluate site feasibility will <u>not</u> be adequate to develop geotechnical design recommendations for the project.

Do not rely on this report if your geotechnical engineer prepared it:

- for a different client;
- for a different project or purpose;
- for a different site (that may or may not include all or a portion of the original site); or
- before important events occurred at the site or adjacent to it; e.g., man-made events like construction or environmental remediation, or natural events like floods, droughts, earthquakes, or groundwater fluctuations.

Note, too, the reliability of a geotechnical-engineering report can be affected by the passage of time, because of factors like changed subsurface conditions; new or modified codes, standards, or regulations; or new techniques or tools. *If you are the least bit uncertain* about the continued reliability of this report, contact your geotechnical engineer before applying the recommendations in it. A minor amount of additional testing or analysis after the passage of time – if any is required at all – could prevent major problems.

Read this Report in Full

Costly problems have occurred because those relying on a geotechnicalengineering report did not read the report in its entirety. Do <u>not</u> rely on an executive summary. Do <u>not</u> read selective elements only. *Read and refer to the report in full.*

You Need to Inform Your Geotechnical Engineer About Change

Your geotechnical engineer considered unique, project-specific factors when developing the scope of study behind this report and developing the confirmation-dependent recommendations the report conveys. Typical changes that could erode the reliability of this report include those that affect:

- the site's size or shape;
- the elevation, configuration, location, orientation, function or weight of the proposed structure and the desired performance criteria;
- the composition of the design team; or
- project ownership.

As a general rule, *always* inform your geotechnical engineer of project or site changes – even minor ones – and request an assessment of their impact. *The geotechnical engineer who prepared this report cannot accept* responsibility or liability for problems that arise because the geotechnical engineer was not informed about developments the engineer otherwise would have considered.

Most of the "Findings" Related in This Report Are Professional Opinions

Before construction begins, geotechnical engineers explore a site's subsurface using various sampling and testing procedures. *Geotechnical engineers can observe actual subsurface conditions only at those specific locations where sampling and testing is performed.* The data derived from that sampling and testing were reviewed by your geotechnical engineer, who then applied professional judgement to form opinions about subsurface conditions throughout the site. Actual sitewide-subsurface conditions may differ – maybe significantly – from those indicated in this report. Confront that risk by retaining your geotechnical engineer to serve on the design team through project completion to obtain informed guidance quickly, whenever needed.

This Report's Recommendations Are Confirmation-Dependent

The recommendations included in this report – including any options or alternatives – are confirmation-dependent. In other words, they are <u>not</u> final, because the geotechnical engineer who developed them relied heavily on judgement and opinion to do so. Your geotechnical engineer can finalize the recommendations *only after observing actual subsurface conditions* exposed during construction. If through observation your geotechnical engineer confirms that the conditions assumed to exist actually do exist, the recommendations can be relied upon, assuming no other changes have occurred. *The geotechnical engineer who prepared this report cannot assume responsibility or liability for confirmation-dependent recommendations if you fail to retain that engineer to perform construction observation.*

This Report Could Be Misinterpreted

Other design professionals' misinterpretation of geotechnicalengineering reports has resulted in costly problems. Confront that risk by having your geotechnical engineer serve as a continuing member of the design team, to:

- confer with other design-team members;
- help develop specifications;
- review pertinent elements of other design professionals' plans and specifications; and
- be available whenever geotechnical-engineering guidance is needed.

You should also confront the risk of constructors misinterpreting this report. Do so by retaining your geotechnical engineer to participate in prebid and preconstruction conferences and to perform constructionphase observations.

Give Constructors a Complete Report and Guidance

Some owners and design professionals mistakenly believe they can shift unanticipated-subsurface-conditions liability to constructors by limiting the information they provide for bid preparation. To help prevent the costly, contentious problems this practice has caused, include the complete geotechnical-engineering report, along with any attachments or appendices, with your contract documents, *but be certain to note* conspicuously that you've included the material for information purposes only. To avoid misunderstanding, you may also want to note that "informational purposes" means constructors have no right to rely on the interpretations, opinions, conclusions, or recommendations in the report. Be certain that constructors know they may learn about specific project requirements, including options selected from the report, only from the design drawings and specifications. Remind constructors that they may perform their own studies if they want to, and be sure to allow enough time to permit them to do so. Only then might you be in a position to give constructors the information available to you, while requiring them to at least share some of the financial responsibilities stemming from unanticipated conditions. Conducting prebid and preconstruction conferences can also be valuable in this respect.

Read Responsibility Provisions Closely

Some client representatives, design professionals, and constructors do not realize that geotechnical engineering is far less exact than other engineering disciplines. This happens in part because soil and rock on project sites are typically heterogeneous and not manufactured materials with well-defined engineering properties like steel and concrete. That lack of understanding has nurtured unrealistic expectations that have resulted in disappointments, delays, cost overruns, claims, and disputes. To confront that risk, geotechnical engineers commonly include explanatory provisions in their reports. Sometimes labeled "limitations," many of these provisions indicate where geotechnical engineers' responsibilities begin and end, to help others recognize their own responsibilities and risks. *Read these provisions closely*. Ask questions. Your geotechnical engineer should respond fully and frankly.

Geoenvironmental Concerns Are Not Covered

The personnel, equipment, and techniques used to perform an environmental study – e.g., a "phase-one" or "phase-two" environmental site assessment – differ significantly from those used to perform a geotechnical-engineering study. For that reason, a geotechnical-engineering report does not usually provide environmental findings, conclusions, or recommendations; e.g., about the likelihood of encountering underground storage tanks or regulated contaminants. *Unanticipated subsurface environmental problems have led to project failures.* If you have not obtained your own environmental information about the project site, ask your geotechnical consultant for a recommendation on how to find environmental risk-management guidance.

Obtain Professional Assistance to Deal with Moisture Infiltration and Mold

While your geotechnical engineer may have addressed groundwater, water infiltration, or similar issues in this report, the engineer's services were not designed, conducted, or intended to prevent migration of moisture – including water vapor – from the soil through building slabs and walls and into the building interior, where it can cause mold growth and material-performance deficiencies. Accordingly, proper implementation of the geotechnical engineer's recommendations will <u>not</u> of itself be sufficient to prevent moisture infiltration. Confront the risk of moisture infiltration by including building-envelope or mold specialists on the design team. Geotechnical engineers are <u>not</u> building-envelope or mold specialists.



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